

Stormwater Analysis

Monarch Drive
Littleton, Massachusetts

Permit Set – April 2022



PREPARED FOR:

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Executive Summary

***In response to peer review comments and further design refinement of the proposed building, updates to the drainage design and report include:**

- The rainfall events utilized in the HydroCAD computer analysis were updated to an NRCS NOAA storm. This provides a localized rainfall event with more recent stormwater events taken into consideration in the statistical analysis that determines the rainfall depths.
- Minor volume changes in ponds 300 and 165 to reflect the existing berm of elevation elevation of 228.65 (previously modeled as 228.50).
- Total Suspended Solids calculations for the CDS stormwater treatment units.
- Expanded Operation and Maintenance Plan and BMP Map.

The proposed site development will be the construction of a 98,000 s.f. industrial building. As the exact usage of the building is not yet determined, the perimeter of the parking/driveway area has been designed so that the southerly end of the building can accommodate either parking or loading bays. Loading bays will be provided at the northerly end of the building under all scenarios.

As this site is in an environmentally sensitive area as it is in the Aquifer Protection district as well as in a priority habitat area. As a result, the water quality volume is based on a 1" first flush and Low Impact Development techniques are preferable.

There are three general design methodologies being used to treat, infiltrate and attenuate runoff from the site. Tree Box Filters will be utilized along the perimeter of the parking areas, two different styles are utilized to provide a curb inlet in the front of the building and a drop inlet along the perimeter. These Tree Box Filters will be interconnected with a subsurface recharge trench that ultimately discharges into recharge basins or infiltration bed.

At the loading dock areas, the pavement pitches to a localized low area where a trench drain will capture the runoff and direct it to a hydrodynamic separator. In the event of a hazardous materials spill, a gate valve is provided prior to the hydrodynamic separator so that the contamination can be contained within the paved area immediately adjacent to the loading docks. Treated runoff from the loading docks as well as overflow from the Tree Filter Boxes is discharged into infiltration basins.

The point of analysis for the site is the northwesterly end of the drainage ditch (now BVW) as it enters the existing pond on Lot 1. A summary table of the flows is below:

HydroCAD Analysis Results				
	Storm Event Discharge Rates (cfs)			
Design Storm Event	2-Year	10-Year	25-Year	100-Year
Existing Conditions	0.04	0.40	0.99	2.60
Proposed Conditions	0.04	0.32	0.94	2.48

As Littleton is a MS4 community with a Stormwater By-law, calculations for Phosphorus removal have been included in these calculations. The total Phosphorus reduction from the developed portions of the site is 89.3 % (60% required)

This design is in full compliance with the MADEP stormwater management standards and incorporates best management practices (BMP's) consistent with low impact development (LID) and incorporates many of the concepts emphasized in LID design.

BMP's utilized:

- Tree Filter Box
- Hydrodynamic Separator
- Infiltration Basin
- Infiltration Trench

Introduction

Excerpt from MADEP Stormwater Management Standards Chapter 1:

In 1996, the Massachusetts Department of Environmental Protection (the “Department” or “MassDEP”) issued the Stormwater Policy that established Stormwater Management Standards aimed at encouraging recharge and preventing stormwater discharges from causing or contributing to the pollution of the surface waters and groundwaters of the Commonwealth. In 1997, MassDEP published the Massachusetts Stormwater Handbook as guidance on the Stormwater Policy. MassDEP has revised the Stormwater Management Standards and Massachusetts Stormwater Handbook to promote increased stormwater recharge, the treatment of more runoff from polluting land uses, low impact development (LID) techniques, pollution prevention, the removal of illicit discharges to stormwater management systems, and improved operation and maintenance of stormwater best management practices (BMPs). MassDEP applies the Stormwater Management Standards pursuant to its authority under the Wetlands Protection Act, M.G.L. c. 131, § 40, and the Massachusetts Clean Waters Act, M.G.L.c. 21, §§ 26-53. The revised Stormwater Management Standards have been incorporated in the Wetlands Protection Act Regulations, 310 CMR 10.05(6)(k) and the Water Quality Certification Regulations, 314 CMR 9.06(6)(a).

Stormwater runoff results from rainfall and snow melt and represents the single largest source responsible for water quality impairments in the Commonwealth’s rivers, lakes, ponds, and marine waters. New and existing development typically adds impervious surfaces and, if not properly managed, may alter natural drainage features, increase peak discharge rates and volumes, reduce recharge to wetlands and streams, and increase the discharge of pollutants to wetlands and water bodies.

The Stormwater Management Standards address water quality (pollutants) and water quantity (flooding, low base flow and recharge) by establishing standards that require the implementation of a wide variety of stormwater management strategies. These strategies include environmentally sensitive site design and LID techniques to minimize impervious surface and land disturbance, source control and pollution prevention, structural BMPs, construction period erosion and sedimentation control, and the long-term operation and maintenance of stormwater management systems.

Narrative – Existing Conditions

The existing site is located at the end of Monarch Drive in Littleton, MA. The proposed site is comprised of Lots 2A and 2B containing 20.08 acres is currently vacant land. The site was formerly mined for gravel and the remaining land has been left with little or no topsoil resulting in sparse vegetation. The soils are A manmade ditch, now qualifying as wetlands, encircles the buildable portion of the site directly adjacent to the shared access driveway, opposite of the existing office building at 1 Monarch Drive. This drainage system flows from the southwest, around the buildable area, through a 24" culvert to the east and loops back to a manmade pond on Lot 1 to the northwest of the site. The end of this drainage ditch, prior to the discharge into the pond is the Point of Analysis for this site.

The surface cover on the front portion of the site is a combination of brush/weeds interspersed with some trees as well as barren soil. This area is being categorized as brush/grass/weeds in poor condition due to the sparse vegetation and exposed soils. Generally, the more established vegetation is located within the 50' buffer to the wetlands and has been classified as wood in poor condition reflective of the thin layer of topsoil and leaf litter. There is some planted and maintained lawn areas, directly adjacent to the access driveway which is considered grass in good condition.

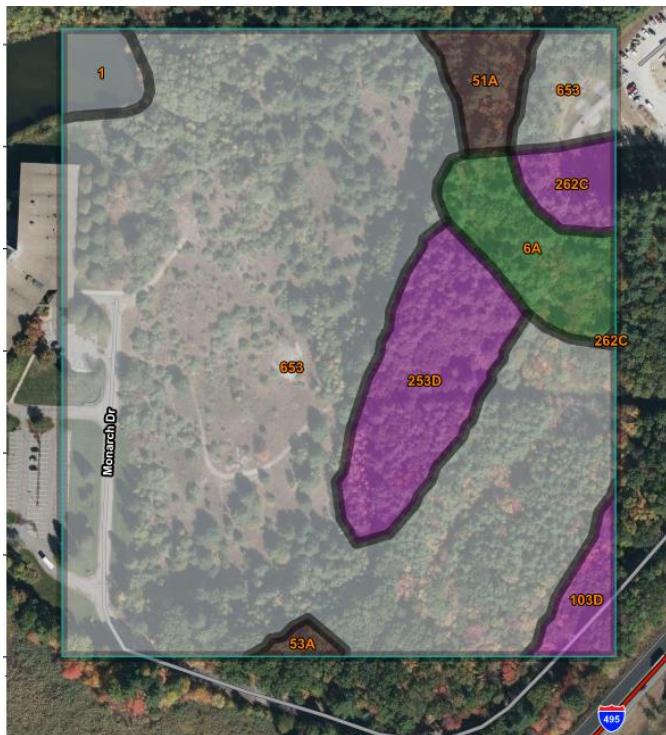
Access to the easterly side of the site is via a gravel road over the culvert. This area is wooded with tall pines and soil testing indicated 3-4" of topsoil, evidence of previous gravel mining operations. There is no shrub or herbaceous layer beneath the trees with thin forest litter, so these woods are considered fair condition.

In general, the site appears to have been graded for a pad development with a large portion of the buildable area at elevations 230 to 234. Elevations of the wetlands are approximately 224. Soil testing performed both for the current project and previous project are consistent with the groundwater table being at elevation 224 or lower.

Soils on this site are Hydrologic Group A containing udorthents and Hinckley loamy sand as indicated on the soils map below:

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
1	Water		0.6	2.0%
6A	Scarboro mucky fine sandy loam, 0 to 3 percent slopes	A/D	1.6	5.3%
51A	Swansea muck, 0 to 1 percent slopes	B/D	0.8	2.7%
53A	Freetown muck, ponded, 0 to 1 percent slopes	B/D	0.2	0.6%
103D	Charlton-Hollis-Rock outcrop complex, 15 to 25 percent slopes	A	0.6	2.2%
253D	Hinckley loamy sand, 15 to 25 percent slopes	A	2.6	8.8%
262C	Quonset sandy loam, 8 to 15 percent slopes	A	0.7	2.2%
653	Udorthents, sandy		22.8	76.3%
Totals for Area of Interest			29.9	100.0%



This site is contained in a mapped habitat area. Under a previous development proposal for a hotel, a large portion of the site was placed in a Conservation Restriction and areas designated for specific uses such as drainage or septic areas. Utilities were installed to serve the building on Lot 1.

Narrative – Proposed Conditions

The proposed site development will be the construction of a 98,000 s.f. industrial building. As the exact usage of the building is not yet determined, the perimeter of the parking/driveway area has been designed so that the southerly end of the building can accommodate either parking or loading bays. Loading bays will be provided at the northerly end of the building under all scenarios.

As this site is in an environmentally sensitive area as it is in the Aquifer Protection district as well as in a priority habitat area. As a result, the water quality volume is based on a 1" first flush and Low Impact Development techniques are preferable.

There are three general design methodologies being used to treat, infiltrate and attenuate runoff from the site. The first is with the use of Tree Filter Boxes. These will be used to capture and pre-treat the runoff from the parking areas and site driveway. There are two basic types of Tree Filter Boxes (TFB) proposed. The first is the traditional TFB where runoff enters the TFB from a curb inlet and the area around the base of the tree is covered in a tree gate. These TFB will be used adjacent to the parking areas at the front (west side) of the building. These areas are more removed from the perimeter of the site and are less likely to intercept young animals.

At the outer perimeter of the parking and loading dock areas, the second type of TFB will be utilized. These TFB will be comprised of an open bottom structure, set just below the elevation of the edge of pavement, dropping 6" to a bark mulch surface surrounding the tree. Parking lot runoff will enter the TFB via a break in the berm. This design will allow the surface surrounding the tree to be visible and if any animals are within the TFB, they can easily be viewed and freed. Both types of TFB will be interconnected with a 12" perforated pipe, set level, to allow recharge.

The catchbasin in the middle of the parking area at the front (west side) of the building must be pre-treated prior to discharge into subsurface chambers. A hydrodynamic separator, with a catchbasin grate will provide the pretreatment and direct the runoff into the chambers for recharge and attenuation.

At each loading dock area, at the north and south ends of the building, the intent is to provide emergency storage should there be any type of spill at the loading docks. The parking slopes from the loading dock to a trench drain at a localized low area. Runoff from the trench drain is routed into a catchbasin then via pipe to a hydrodynamic separator. Between the manhole and separator there will be a shut off valve. The area around the trench drain will contain a spill until it can be cleaned. From the hydrodynamic separator, the pretreated runoff will be directed into the infiltration basins on the easterly side of the building.

As Littleton is a MS4 community with a Stormwater By-law, calculations for Phosphorus removal have been included in these calculations.

This design is in full compliance with the MADEP stormwater management standards and incorporates best management practices (BMP's) consistent with low impact development (LID) and incorporates many of the concepts emphasized in LID design.

BMPs utilized:

- Tree Filter Box
- Hydrodynamic Separator
- Infiltration Basin
- Infiltration Trench

LID/Environmentally Sensitive Design Techniques utilized (Volume 1- Chapter 1):

- *Maintain as much of the pre-development vegetation as possible*
- *Maintain natural buffers and drainage ways*
- *Utilize country style drainage*

Narrative – Hydrologic Analysis

The point of analysis for the hydrologic analysis is the outlet from the existing drainage ditch, shown as Reach 3 in both the Pre and Post Development calculations.

In order to achieve both the attenuation of flow rates and a reduction in the total Phosphorus from the site recharge is required. This design has maximized the recharge to the extent practicable in order to achieve no increase in the rate of runoff for the 2 year storm event. The infiltration and stormwater basin system has been designed for overflow at the surface in order to meet the 50' no disturbance buffer zone to the wetlands. As a result, the surface stormwater basins do not overflow in the 2, 10 or 25 year storm events.

The soils on the site are a well sorted sand, with a percolation rate in excess of 2 minutes per inch. It is anticipated that runoff infiltrating into the groundwater will migrate to the same wetlands, helping to sustain the hydrology of those wetlands, despite the decrease in the rate of runoff.

The wooded area, to the east of the culvert crossing will be cleared for the septic system installation. The existing woods are considered to be Woods, fair condition due to the 3-4" of topsoil, absence of understory vegetation, both herbaceous and shrubs, and a very minimal surface litter. The Curve Number for these conditions, with A soils is 43. Under post development, the areas for the leaching field will be stabilized with 6" of loam and a conservation grass seed mix. As this area is not directly adjacent to the building, it is anticipated that it will be mowed several times a year, not weekly as the grass areas adjacent to the building. Once this area is fully vegetated, will likely have a combination of grasses, weeds and some brush given the presence of weed seed in the adjacent natural areas, in fair condition due to the excessively drained soils. Brush/weed/grass mix in fair condition has a curve number of 35. As a result, no changes are anticipated in the runoff from this portion of the property.

Documenting Compliance

Standard 1 - No new stormwater conveyances (e.g. outfalls) may discharge untreated stormwater directly to or cause erosion in wetlands or waters of the Commonwealth.

No untreated outfalls are proposed.

Standard 2 - Stormwater management systems shall be designed so that the post-development peak discharge rates do not exceed pre-development peak discharge rates...To prevent storm damage and downstream and off-site flooding, Standard 2 requires that the post-development peak discharge rate is equal to or less than the pre-development rate from the 2-year and the 10-year 24-hour storms...Proponents must also evaluate the impact of peak discharges from the 100-year 24-hour storm. If this evaluation shows that increased off-site flooding will result from peak discharges from the 100-year 24-hour storms, BMPs must also be provided to attenuate these discharges.

The post development runoff calculations demonstrate no increase in the rate of runoff for any of the storms.

Standard 3 - Loss of annual recharge to groundwater shall be eliminated or minimized through the use of infiltration measures including environmentally sensitive site design, low impact development techniques, stormwater best management practices, and good operation and maintenance. At a minimum, the annual recharge from the post-development site shall approximate the annual recharge from pre-development conditions based on soil type. This Standard is met when the stormwater management system is designed to infiltrate the required recharge volume as determined in accordance with the Massachusetts Stormwater Handbook.

Tributary Impervious area = 203,545 sq.ft. (buildings and pavement)

Class A soils = 0.6 inches x impervious area

Required recharge (Rv)= 203,545 sq.ft. x 0.6 inches x 1ft/12in = **10,177 cubic feet required**

Capture Area Adjustment:

Impervious surfaces tributary to Basins and Chambers = $132,540 + 27160 + 22,330 = 182,030$

Ratio of total impervious to impervious to recharge = $203,545 / 182,030 = 1.12$

Adjusted minimum required recharge = $10,177 \times 1.12 = 11,398 \text{ cubic feet required}$

Static Recharge Provided (see HydroCAD output for details)

Infiltration Basin 1 (below overflow elevation 229.80) = **29,380 c.f.**

Infiltration Basin 2 & 3 (below overflow elevation 228.65) = **4,986 c.f.**

Infiltration Chambers (below outlet elevation of 228.0) = **2,212 c.f.**

Total provided= 36,578 c.f. < 11,398

Drawdown times:

To simplify, only consider infiltration in basins, excluding recharge occurring between tree filter boxes

Infiltration Basin 1

Rv= $132,540 \times 0.6 \times 1 \text{ ft}/12\text{in} = 6627 \text{ c.f.}$

Time= $6627 \text{ c.f.} / (8.27 \text{ in}/\text{hr})(1\text{ft}/12\text{in})(4545 \text{ s.f.}) = 2.1 \text{ hours}$

Infiltration Basins 2 and 3

Rv= $27160 \times 0.6 \times 1/12 = 1358 \text{ c.f.}$

Time= $1358 \text{ c.f.} / (8.27 \text{ in}/\text{hr}) \times 0.6 \times 1/12 \times 1195 = 2.75 \text{ hours}$

Infiltration Chambers

Rv= $22,330 \times 0.6 \times 1/12 = 1117 \text{ c.f.}$

Time= $1117 \text{ c.f.} / (8.27 \text{ in}/\text{hr}) \times 0.6 \times 1/12 \times 1544 \text{ s.f.} = 1.74 \text{ hours}$

Groundwater Mounding:

Use USGS Groundwater Mounding Spreadsheet with the following parameters

Rv= Recharge Volume

Recharge Rate = Rv applied over bottom for 72 hours = $Rv / (\text{bot area s.f.})(3 \text{ days})$

Sy for sand= 0.26

K Horizontal Hydraulic Conductivity for coarse sand = 55

X= ½ length basin

Y=1/2 width basin

T= duration of flow = 3 days

Hi= initial thickness of saturated zone (assume 20' min. since area is an Aquifer District)

Infiltration Basin 1

R= $6627 \text{ c.f.} / (4545 \text{ s.f.}) \times (3 \text{ days}) = 0.49$

Resulting Groundwater mound using Rv is 0.733'

Input Values		use consistent units (e.g. feet & days OR inches & hours)			Conversion Table	
			inch/hour	feet/day		
0.4900	R	Recharge (infiltration) rate (feet/day)	0.67	1.33		
0.260	Sy	Specific yield, Sy (dimensionless, between 0 and 1)				
55.00	K	Horizontal hydraulic conductivity, Kh (feet/day)*	2.00	4.00	In the report accompanying this spreadsheet (USGS SIR 2010-5102), vertical soil permeability (ft/d) is assumed to be one-tenth horizontal	
51.000	x	1/2 length of basin (x direction, in feet)				
22.000	y	1/2 width of basin (y direction, in feet)				
3.000	t	duration of infiltration period (days)	hours	days	36	1.50 hydraulic conductivity (ft/d).
15.000	hi(0)	initial thickness of saturated zone (feet)				
15.733	h(max)	maximum thickness of saturated zone (beneath center of basin at end of infiltration period)				
0.733	Δh(max)	maximum groundwater mounding (beneath center of basin at end of infiltration period)				

Infiltration Basins 2 and 3

$$R = 1358 \text{ c.f./3 days (1195 s.f.)} = 0.37$$

Resulting Groundwater mound using Rv is 0.187

Input Values		use consistent units (e.g. feet & days OR inches & hours)			Conversion Table	
			inch/hour	feet/day		
0.3700	R	Recharge (infiltration) rate (feet/day)	0.67	1.33		
0.260	Sy	Specific yield, Sy (dimensionless, between 0 and 1)				
55.00	K	Horizontal hydraulic conductivity, Kh (feet/day)*	2.00	4.00	In the report accompanying this spreadsheet (USGS SIR 2010-5102), vertical soil permeability (ft/d) is assumed to be one-tenth horizontal	
41.000	x	1/2 length of basin (x direction, in feet)				
7.500	y	1/2 width of basin (y direction, in feet)				
3.000	t	duration of infiltration period (days)	hours	days	36	1.50 hydraulic conductivity (ft/d).
15.000	hi(0)	initial thickness of saturated zone (feet)				
15.187	h(max)	maximum thickness of saturated zone (beneath center of basin at end of infiltration period)				
0.187	Δh(max)	maximum groundwater mounding (beneath center of basin at end of infiltration period)				

Infiltration Chambers

$$R = 1117 \text{ c.f./3 days (1544 s.f.)} = 0.03$$

Resulting Groundwater mound using Rv is 0.02'

Input Values		use consistent units (e.g. feet & days OR inches & hours)			Conversion Table	
			inch/hour	feet/day		
0.0300	R	Recharge (infiltration) rate (feet/day)	0.67	1.33		
0.260	Sy	Specific yield, Sy (dimensionless, between 0 and 1)				
55.00	K	Horizontal hydraulic conductivity, Kh (feet/day)*	2.00	4.00	In the report accompanying this spreadsheet (USGS SIR 2010-5102), vertical soil permeability (ft/d) is assumed to be one-tenth horizontal	
33.000	x	1/2 length of basin (x direction, in feet)				
12.000	y	1/2 width of basin (y direction, in feet)				
3.000	t	duration of infiltration period (days)	hours	days	36	1.50 hydraulic conductivity (ft/d).
15.000	hi(0)	initial thickness of saturated zone (feet)				
15.020	h(max)	maximum thickness of saturated zone (beneath center of basin at end of infiltration period)				
0.020	Δh(max)	maximum groundwater mounding (beneath center of basin at end of infiltration period)				

Standard 4 - Stormwater management systems shall be designed to remove 80% of the average annual post-construction load of Total Suspended Solids (TSS).

For purposes of Standards 3 and 4, impervious surfaces include roads, rooftops, parking lots, and sidewalks, when they are paved with concrete, asphalt, or brick pavers. (Volume 3, Chapter 1, Page 15)

Parking lot areas		Removal Rate	Remains	
Pretreatment	Tree Filter Box	85%	15%	
Treatment	Infiltration	80%	3%	
Final Rate			97%	removal

* Tree Filter Box provided at a rate of 1/0.1 Ac. Impervious or less in compliance with UNH Stormwater Center Guidelines

Loading Dock Areas		Removal Rate	Remains	
Pretreatment	Hydrodynamic separator	96%	4%	
Treatment	Infiltration	80%	1%	
Final Rate			99%	removal

CTB front of building		Removal Rate	Remains	
Pretreatment	Hydrodynamic separator	96%	4%	
Treatment	Infiltration	80%	1%	
Final Rate			99%	removal

Standard 5 - For land uses with higher potential pollutant loads, source control and pollution prevention shall be implemented in accordance with the Massachusetts Stormwater Handbook to eliminate or reduce the discharge of stormwater runoff from such land uses to the maximum extent practicable. If through source control and/or pollution prevention all land uses with higher potential pollutant loads cannot be completely protected from exposure to rain, snow, snow melt, and stormwater runoff, the proponent shall use the specific structural stormwater BMPs determined by the Department to be suitable for such uses as provided in the Massachusetts Stormwater Handbook. Stormwater discharges from land uses with higher potential pollutant loads shall also comply with the requirements of the Massachusetts Clean Waters Act, M.G.L. c. 21, §§ 26-53 and the regulations promulgated thereunder at 314 CMR 3.00, 314 CMR 4.00 and 314 CMR 5.00.

The project does not qualify as a LUHPPL.

Standard 6 - Stormwater discharges within the Zone II or Interim Wellhead Protection Area of a public water supply, and stormwater discharges near or to any other critical area, require the use of the specific source control and pollution prevention measures and the specific structural stormwater best management practices determined by the Department to be suitable for managing discharges to such areas, as provided in the Massachusetts Stormwater Handbook. A discharge is near a critical area if there is a strong likelihood of a significant impact occurring to said area, taking into account site-specific factors. Stormwater discharges to Outstanding Resource Waters and Special Resource Waters shall be removed and set back from the receiving water or wetland and receive the highest and best practical method of treatment. A "storm water discharge" as defined in 314 CMR 3.04(2)(a)1 or (b) to an

Outstanding Resource Water or Special Resource Water shall comply with 314 CMR 3.00 and 314 CMR 4.00. Stormwater discharges to a Zone I or Zone A are prohibited unless essential to the operation of a public water supply.

This site is within a mapped Priority Habitat area. All discharge points are outside of the existing Conservation Restriction Area. The drainage design has incorporated multiple infiltration basins where the outlet utilizes natural low points or overflow weirs located outside the limits of the CR. The exception is the discharges near the cul-de-sac of Monarch Drive where existing grades in Monarch Drive are low, eliminating the ability to daylight the drainage system outside of the 50' vegetative buffer to the wetlands.

Standard 7 - A redevelopment project is required to meet the following Stormwater Management Standards only to the maximum extent practicable: Standard 2, Standard 3, and the pretreatment and structural best management practice requirements of Standards 4, 5, and 6. Existing stormwater discharges shall comply with Standard 1 only to the maximum extent practicable. A redevelopment project shall also comply with all other requirements of the Stormwater Management Standards and improve existing conditions.

The project is not proposed as redevelopment.

Standard 8 - A plan to control construction-related impacts including erosion, sedimentation and other pollutant sources during construction and land disturbance activities (construction period erosion, sedimentation, and pollution prevention plan) shall be developed and implemented.

See site plans included with this application.

Standard 9 - A long-term operation and maintenance plan shall be developed and implemented to ensure that stormwater management systems function as designed.

See the Operation and Maintenance Plan included in this document.

Standard 10 - All illicit discharges to the stormwater management system are prohibited.

Illicit Discharge Compliance Statement

To the best of my knowledge no illicit discharges currently exist on the site and no future illicit discharge will be allowed, including wastewater discharges and discharges of stormwater contaminated by contact with process wastes, raw materials, toxic pollutants, hazardous substances, oil, or grease.

Signature of Owner

Date

To be completed and submitted prior to the start of construction.

PHOSPHORUS REMOVAL:

MS4 requirements for 60% Total Phosphorous Removal.

IA= Impervious Area

PA= Pervious Area

Calculations:

BMP Design Volume = storage volume in basin which is available for recharge

IA Rainfall depth= depth of rainfall that would generate the BMP volume in the Basin.

PA BMP Volume= volume generated by the pervious areas using the IA rainfall depth and Chart 3-3 using soil type and surface cover to generate the volume (Excel chart for each BMP)

P Load= Phosphorus load based on surface cover (Appendix F, Attachment 3, Pg. 10)

BMP Reduction (%) = BMP Performance curve using infiltration rate and depth of runoff from the IA

Basin 1 (Pond 165):

Basin 1 has

Design Vol=29,380 c.f.

Infiltration Rate=8.27

Tributary Impervious= 132,540; Pervious (landscaped)= 27,585 s.f.

IA Rainfall Depth= $(29,380 \text{ c.f.}) / 132,540 \text{ s.f. imp} = 0.22 \text{ feet} = 2.66 \text{ inches}$

Note: Table 3-15 provides runoff depths for pervious surfaces with initial rainfall depths up to 2". The 100% P removal occurs with rainfall depth of 1.5" which is less than the IA rainfall depth. Therefore, these calculations will determine the minimum volume needed to achieve 100% Phosphorus removal.

From BMP Performance Curve: Infiltration Basin (Infiltration Rate = 8.27 in/hr), 100% Pollutant level is achieved with a 1.5" Depth of Runoff from the IA.

IA Rainfall Depth = 1.5"

IA Volume= IA depth (in)x 1'/12"x IA = 1.5"x1'/12"x 132,540 s.f.= 16,568 c.f

PA use Rainfall Depth 1.5" and excel spreadsheet to calculated volume of pervious areas= 322

Basin Volume for 100% P Reduction (1.5" Rainfall Depth) = IA Volume + PA Volume = 16,890 c.f. < 29,380c.f., therefore 100% reduction is achieved.

Basin 2 and 3 (Ponds 300 and 301):

Basins 2 and 3 have:

Design Vol=4,986 c.f.

Infiltration Rate=8.27

Tributary Impervious= 27,160; Pervious (landscaped)= 33,305 s.f.

IA Rainfall Depth= $(4,986 \text{ c.f.}) / 27,160 \text{ s.f. imp} = 0.183 \text{ feet} = 2.20 \text{ inches}$

Note: Table 3-15 provides runoff depths for pervious surfaces with initial rainfall depths up to 2". The 100% P removal occurs with rainfall depth of 1.5" which is less than the IA rainfall depth. Therefore, these calculations will determine the minimum volume needed to achieve 100% Phosphorus removal.

From BMP Performance Curve: Infiltration Basin (Infiltration Rate = 8.27 in/hr), 100% Pollutant level is achieved with a 1.5" Depth of Runoff from the IA.

IA Rainfall Depth = 1.5"

IA Volume= IA depth (in)x 1'/12"x IA = 1.5"x1'/12"x 27,160 s.f.= 3,395 c.f

PA use Rainfall Depth 1.5" and excel spreadsheet to calculated volume of pervious areas= 389

Basin Volume for 100% P Reduction (1.5" Rainfall Depth) = IA Volume + PA Volume = 3,784 c.f. < 4,115 c.f., therefore 100% reduction is achieved.

Infiltration Trenches and Infiltration Chamber (Ponds 220 and 222):

Design Vol=3,777 c.f.

Infiltration Rate=8.27

Tributary Impervious= 22,330; Pervious (landscaped)= 3845 s.f.

IA Rainfall Depth= (3,777 c.f.)/22,330 s.f. imp= 0.169 feet =2.03 inches

Note: Table 3-9 provides runoff depths for pervious surfaces with initial rainfall depths up to 2". The 100% P removal occurs with rainfall depth of 1.5" which is less than the IA rainfall depth. Therefore, these calculations will determine the minimum volume needed to achieve 100% Phosphorus removal.

From BMP Performance Curve: Infiltration Basin (Infiltration Rate = 8.27 in/hr), 100% Pollutant level is achieved with a 1.5" Depth of Runoff from the IA.

IA Rainfall Depth = 1.5"

IA Volume= IA depth (in)x 1'/12"x IA = 1.5"x1'/12"x 22,330 s.f.= 2,791 c.f

PA use Rainfall Depth 1.5" and excel spreadsheet to calculated volume of pervious areas= 45

Basin Volume for 100% P Reduction (1.5" Rainfall Depth) = IA Volume + PA Volume = 2,836 c.f. < 3,777 c.f., therefore 100% reduction is achieved.

TOTAL REDUCTION OF PHOSPHORUS LOAD SITEWIDE = 89.38 % >60%

Supporting Data – Phosphorus Removal

Stage-Area-Storage for Pond 165: infiltration basin

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
226.00	4,515	0	228.60	9,015	17,289
226.05	4,592	228	228.65	9,112	17,743
226.10	4,668	459	228.70	9,209	18,201
226.15	4,745	694	228.75	9,306	18,664
226.20	4,821	934	228.80	9,403	19,131
226.25	4,898	1,177	228.85	9,499	19,604
226.30	4,974	1,423	228.90	9,596	20,081
226.35	5,050	1,674	228.95	9,693	20,563
226.40	5,127	1,928	229.00	9,790	21,051
226.45	5,203	2,187	229.05	9,888	21,542
226.50	5,280	2,449	229.10	9,945	22,037
226.55	5,357	2,715	229.15	10,023	22,536
226.60	5,433	2,984	229.20	10,101	23,040
226.65	5,510	3,258	229.25	10,179	23,547
226.70	5,586	3,535	229.30	10,257	24,057
226.75	5,663	3,817	229.35	10,334	24,572
226.80	5,739	4,102	229.40	10,412	25,091
226.85	5,815	4,390	229.45	10,490	25,613
226.90	5,892	4,683	229.50	10,568	26,140
226.95	5,968	4,980	229.55	10,645	26,670
227.00	6,045	5,280	229.60	10,723	27,204
227.05	6,135	5,585	229.65	10,801	27,742
227.10	6,226	5,894	229.70	10,878	28,284
227.15	6,316	6,207	229.75	10,956	28,830
227.20	6,407	6,525	229.80	11,034	29,380
227.25	6,497	6,848	229.85	11,112	29,934
227.30	6,587	7,175	229.90	11,190	30,491
227.35	6,678	7,506	229.95	11,267	31,053
227.40	6,768	7,843	230.00	11,345	31,618
227.45	6,859	8,183			
227.50	6,949	8,529			
227.55	7,039	8,878			
227.60	7,130	9,232			
227.65	7,220	9,591			
227.70	7,311	9,954			
227.75	7,401	10,322			
227.80	7,491	10,695			
227.85	7,582	11,071			
227.90	7,672	11,453			
227.95	7,763	11,839			
228.00	7,853	12,229			
228.05	7,950	12,624			
228.10	8,047	13,024			
228.15	8,144	13,429			
228.20	8,240	13,838			
228.25	8,337	14,253			
228.30	8,434	14,672			
228.35	8,531	15,096			
228.40	8,628	15,525			
228.45	8,725	15,959			
228.50	8,822	16,398			
228.55	8,918	16,841			

Stage-Area-Storage for Pond 220: Infiltration Chambers

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
226.00	1,556	0	228.60	1,556	2,782
226.05	1,556	31	228.65	1,556	2,815
226.10	1,556	62	228.70	1,556	2,847
226.15	1,556	93	228.75	1,556	2,878
226.20	1,556	125	228.80	1,556	2,909
226.25	1,556	156	228.85	1,556	2,940
226.30	1,556	187	228.90	1,556	2,971
226.35	1,556	218	228.95	1,556	3,002
226.40	1,556	249	229.00	1,556	3,034
226.45	1,556	280	229.05	1,556	3,065
226.50	1,556	311	229.10	1,556	3,096
226.55	1,556	380	229.15	1,556	3,127
226.60	1,556	448	229.20	1,556	3,158
226.65	1,556	515			
226.70	1,556	582			
226.75	1,556	649			
226.80	1,556	716			
226.85	1,556	782			
226.90	1,556	848			
226.95	1,556	915			
227.00	1,556	981			
227.05	1,556	1,046			
227.10	1,556	1,111			
227.15	1,556	1,176			
227.20	1,556	1,240			
227.25	1,556	1,304			
227.30	1,556	1,367			
227.35	1,556	1,431			
227.40	1,556	1,493			
227.45	1,556	1,556			
227.50	1,556	1,618			
227.55	1,556	1,680			
227.60	1,556	1,742			
227.65	1,556	1,803			
227.70	1,556	1,863			
227.75	1,556	1,923			
227.80	1,556	1,982			
227.85	1,556	2,041			
227.90	1,556	2,099			
227.95	1,556	2,156			
228.00	1,556	2,212			
228.05	1,556	2,267			
228.10	1,556	2,322			
228.15	1,556	2,375			
228.20	1,556	2,428			
228.25	1,556	2,479			
228.30	1,556	2,529			
228.35	1,556	2,577			
228.40	1,556	2,623			
228.45	1,556	2,668			
228.50	1,556	2,709			
228.55	1,556	2,747			

Stage-Area-Storage for Pond 222: Tree Filter Infiltration

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
227.00	690	0	228.04	690	403
227.02	690	5	228.06	690	410
227.04	690	9	228.08	690	417
227.06	690	14	228.10	690	423
227.08	690	19	228.12	690	430
227.10	690	24	228.14	690	436
227.12	690	29	228.16	690	442
227.14	690	35	228.18	690	448
227.16	690	40	228.20	690	454
227.18	690	46	228.22	690	459
227.20	690	52	228.24	690	464
227.22	690	58	228.26	690	470
227.24	690	65	228.28	690	474
227.26	690	71	228.30	690	479
227.28	690	78	228.32	690	484
227.30	690	85	228.34	690	489
227.32	690	93	228.36	690	493
227.34	690	100	228.38	690	498
227.36	690	108	228.40	690	502
227.38	690	116	228.42	690	507
227.40	690	124	228.44	690	512
227.42	690	133	228.46	690	516
227.44	690	141	228.48	690	521
227.46	690	150	228.50	690	525
227.48	690	158	228.52	690	530
227.50	690	167	228.54	690	535
227.52	690	176	228.56	690	539
227.54	690	185	228.58	690	544
227.56	690	194	228.60	690	548
227.58	690	203	228.62	690	553
227.60	690	212	228.64	690	558
227.62	690	221	228.66	690	562
227.64	690	230	228.68	690	567
227.66	690	239	228.70	690	571
227.68	690	248	228.72	690	576
227.70	690	257	228.74	690	581
227.72	690	266	228.76	690	585
227.74	690	276	228.78	690	590
227.76	690	285	228.80	690	594
227.78	690	294	228.82	690	599
227.80	690	303	228.84	690	604
227.82	690	311	228.86	690	608
227.84	690	320	228.88	690	613
227.86	690	329	228.90	690	617
227.88	690	338	228.92	690	622
227.90	690	346	228.94	690	626
227.92	690	355	228.96	690	631
227.94	690	363	228.98	690	636
227.96	690	372	229.00	690	640
227.98	690	380			
228.00	690	388			
228.02	690	395			

Stage-Area-Storage for Pond 300: Infiltration 1

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
227.00	900	0	228.04	2,113	1,486
227.02	920	18	228.06	2,214	1,529
227.04	940	37	228.08	2,316	1,575
227.06	961	56	228.10	2,417	1,622
227.08	981	75	228.12	2,518	1,671
227.10	1,001	95	228.14	2,619	1,723
227.12	1,021	115	228.16	2,720	1,776
227.14	1,042	136	228.18	2,821	1,831
227.16	1,062	157	228.20	2,923	1,889
227.18	1,082	178	228.22	3,024	1,948
227.20	1,102	200	228.24	3,125	2,010
227.22	1,122	222	228.26	3,226	2,073
227.24	1,143	245	228.28	3,327	2,139
227.26	1,163	268	228.30	3,428	2,206
227.28	1,183	292	228.32	3,530	2,276
227.30	1,203	315	228.34	3,631	2,348
227.32	1,224	340	228.36	3,732	2,421
227.34	1,244	364	228.38	3,833	2,497
227.36	1,264	390	228.40	3,934	2,575
227.38	1,284	415	228.42	4,035	2,654
227.40	1,304	441	228.44	4,137	2,736
227.42	1,325	467	228.46	4,238	2,820
227.44	1,345	494	228.48	4,339	2,905
227.46	1,365	521	228.50	4,440	2,993
227.48	1,385	548	228.52	4,679	3,084
227.50	1,406	576	228.54	4,918	3,180
227.52	1,426	605	228.56	5,157	3,281
227.54	1,446	633	228.58	5,396	3,387
227.56	1,466	663	228.60	5,635	3,497
227.58	1,486	692	228.62	5,874	3,612
227.60	1,507	722	228.64	6,113	3,732
227.62	1,527	752	228.66	6,352	3,857
227.64	1,547	783	228.68	6,591	3,986
227.66	1,567	814	228.70	6,830	4,120
227.68	1,587	846	228.72	7,069	4,259
227.70	1,608	878	228.74	7,308	4,403
227.72	1,628	910	228.76	7,548	4,552
227.74	1,648	943	228.78	7,787	4,705
227.76	1,668	976	228.80	8,026	4,863
227.78	1,689	1,010	228.82	8,265	5,026
227.80	1,709	1,044	228.84	8,504	5,194
227.82	1,729	1,078	228.86	8,743	5,366
227.84	1,749	1,113	228.88	8,982	5,543
227.86	1,769	1,148	228.90	9,221	5,725
227.88	1,790	1,183	228.92	9,460	5,912
227.90	1,810	1,219	228.94	9,699	6,104
227.92	1,830	1,256	228.96	9,938	6,300
227.94	1,850	1,293	228.98	10,177	6,501
227.96	1,871	1,330	229.00	10,416	6,707
227.98	1,891	1,367			
228.00	1,911	1,406			
228.02	2,012	1,445			

Stage-Area-Storage for Pond 301: Infiltration 1

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
227.00	500	0	228.04	837	696
227.02	507	10	228.06	843	713
227.04	513	20	228.08	849	729
227.06	520	31	228.10	855	746
227.08	526	41	228.12	861	764
227.10	532	52	228.14	867	781
227.12	539	62	228.16	873	798
227.14	545	73	228.18	879	816
227.16	552	84	228.20	885	833
227.18	559	95	228.22	891	851
227.20	565	106	228.24	897	869
227.22	571	118	228.26	903	887
227.24	578	129	228.28	910	905
227.26	584	141	228.30	916	924
227.28	591	153	228.32	923	942
227.30	598	165	228.34	929	960
227.32	604	177	228.36	936	979
227.34	611	189	228.38	942	998
227.36	617	201	228.40	949	1,017
227.38	623	213	228.42	956	1,036
227.40	630	226	228.44	962	1,055
227.42	636	239	228.46	969	1,074
227.44	643	251	228.48	975	1,094
227.46	650	264	228.50	982	1,113
227.48	656	277	228.52	988	1,133
227.50	663	291	228.54	995	1,153
227.52	669	304	228.56	1,001	1,173
227.54	675	317	228.58	1,008	1,193
227.56	682	331	228.60	1,014	1,213
227.58	689	345	228.62	1,021	1,233
227.60	695	358	228.64	1,027	1,254
227.62	702	372	228.66	1,034	1,275
227.64	708	387	228.68	1,040	1,295
227.66	714	401	228.70	1,047	1,316
227.68	721	415	228.72	1,054	1,337
227.70	727	430	228.74	1,060	1,358
227.72	734	444	228.76	1,067	1,380
227.74	741	459	228.78	1,073	1,401
227.76	747	474	228.80	1,080	1,423
227.78	754	489	228.82	1,086	1,444
227.80	760	504	228.84	1,093	1,466
227.82	766	519	228.86	1,099	1,488
227.84	773	535	228.88	1,106	1,510
227.86	780	550	228.90	1,112	1,532
227.88	786	566	228.92	1,119	1,554
227.90	793	582	228.94	1,125	1,577
227.92	799	598	228.96	1,132	1,599
227.94	805	614	228.98	1,138	1,622
227.96	812	630	229.00	1,145	1,645
227.98	818	646			
228.00	825	663			
228.02	831	679			

Appendix F Attachment 3

Table 3-1: Average annual distinct phosphorus load (P Load) export rates for use in estimating phosphorus load reduction credits the MA MS4 Permit

Phosphorus Source Category by Land Use	Land Surface Cover	P Load Export Rate, lbs/acre/year	P Load Export Rate, kg/ha/yr
Commercial (Com) and Industrial (Ind)	Directly connected impervious	1.78	2.0
	Pervious	See* DevPERV	See* DevPERV
Multi-Family (MFR) and High-Density Residential (HDR)	Directly connected impervious	2.32	2.6
	Pervious	See* DevPERV	See* DevPERV
Medium -Density Residential (MDR)	Directly connected impervious	1.96	2.2
	Pervious	See* DevPERV	See* DevPERV
Low Density Residential (LDR) - "Rural"	Directly connected impervious	1.52	1.7
	Pervious	See* DevPERV	See* DevPERV
Highway (HWY)	Directly connected impervious	1.34	1.5
	Pervious	See* DevPERV	See* DevPERV
Forest (For)	Directly connected impervious	1.52	1.7
	Pervious	0.13	0.13
Open Land (Open)	Directly connected impervious	1.52	1.7
	Pervious	See* DevPERV	See* DevPERV
Agriculture (Ag)	Directly connected impervious	1.52	1.7
	Pervious	0.45	0.5
*Developed Land Pervious (DevPERV)- Hydrologic Soil Group A	Pervious	0.03	0.03
*Developed Land Pervious (DevPERV)- Hydrologic Soil Group B	Pervious	0.12	0.13
*Developed Land Pervious (DevPERV) - Hydrologic Soil Group C	Pervious	0.21	0.24
*Developed Land Pervious (DevPERV) - Hydrologic Soil Group C/D	Pervious	0.29	0.33
*Developed Land Pervious (DevPERV) - Hydrologic Soil Group D	Pervious	0.37	0.41

VMD MONARCH DRIVE INDUSTRIAL DEVELOPMENT

PHOSPHORUS REMOVAL CALCULATIONS

Basin Number	IMPERVIOUS				Soil Type	Forest/ woods				Lawn/Landscaped Areas				Total P	100% Reduction of Total P		
	S.F	Ac.	P load Chart 3-1	Rainfall Depth for 100%		S.F	Ac.	P load Chart 3-1	Runoff depth Chart 3-3	Runoff Volume	S.F	Ac.	P load Chart 3-1	Runoff depth Chart 3-3			
Basin 1	132,540	3.043	5.96	1.50	A	0	0.000	0.00	0.14	0	27,585	0.633	0.02	0.14	322		
					B	0	0.000	0.00	0.22	0	0	0.000	0.00	0.22	0		
					C	0	0.000	0.00	0.69	0	0	0.000	0.00	0.69	0		
					D	0	0.000	0.00	0.89	0	0	0.000	0.00	0.89	0		
Totals		3.043	5.96			0	0.000	0.00		0	27585	0.633	0.02		322	5.98	5.98

PA Total Runoff Volume 322

Basin Number	IMPERVIOUS				Soil Type	Forest/ woods				Lawn/Landscaped Areas				Total P	100% Reduction of Total P		
	S.F	Ac.	P load Chart 3-1	Rainfall Depth for 100%		S.F	Ac.	P load Chart 3-1	Runoff depth Chart 3-3	Runoff Volume	S.F	Ac.	P load Chart 3-1	Runoff depth Chart 3-3			
Basin 2 and 3	27,160	0.624	1.22	1.50	A	0	0.000	0.00	0.14	0	33,305	0.765	0.02	0.14	389		
					B	0	0.000	0.00	0.22	0	0	0.000	0.00	0.22	0		
					C	0	0.000	0.00	0.69	0	0	0.000	0.00	0.69	0		
					D	0	0.000	0.00	0.89	0	0	0.000	0.00	0.89	0		
Totals		0.624	1.22			0	0.000	0.00		0	33305	0.765	0.02		389	1.25	1.25

PA Total Runoff Volume 389

Basin Number	IMPERVIOUS				Soil Type	Forest/ woods				Lawn/Landscaped Areas				Total P	100% Reduction of Total P		
	S.F	Ac.	P load Chart 3-1	Rainfall Depth for 100%		S.F	Ac.	P load Chart 3-1	Runoff depth Chart 3-3	Runoff Volume	S.F	Ac.	P load Chart 3-1	Runoff depth Chart 3-3			
Infiltration Trench and Chambers	22,330	0.513	1.00	1.50	A	0	0.000	0.00	0.14	0	3,845	0.088	0.00	0.14	45		
					B	0	0.000	0.00	0.22	0	0	0.000	0.00	0.22	0		
					C	0	0.000	0.00	0.69	0	0	0.000	0.00	0.69	0		
					D	0	0.000	0.00	0.89	0	0	0.000	0.00	0.89	0		
Totals		0.513	1.00			0	0.000	0.00		0	3845	0.088	0.00		45	1.01	1.01

PA Total Runoff Volume 45

PHOSPHORUS LOAD FOR ALL DISTURBED AREAS OF SITE															
Basin Number	IMPERVIOUS			Soil Type	Forest			Lawn/Landscaped Areas			Total P	Total P Reduction	Percent of Reduction		
S.F	Ac.	P load		S.F	Ac.	P load	S.F	Ac.	P load						
Entire Site	203545	4.673	9.16	A	0	0.000	0.00	87400	2.006	0.06					
				B	0	0.00	0.00	0	0.000	0.00					
				C	0	0.00	0.00	0	0.000	0.00					
				D	0	0.00	0.00	0	0.000	0.00					
Totals		4.673	9.16		0	0.00	0.00	87400	2.006	0.06	9.22	8.24	89.38		

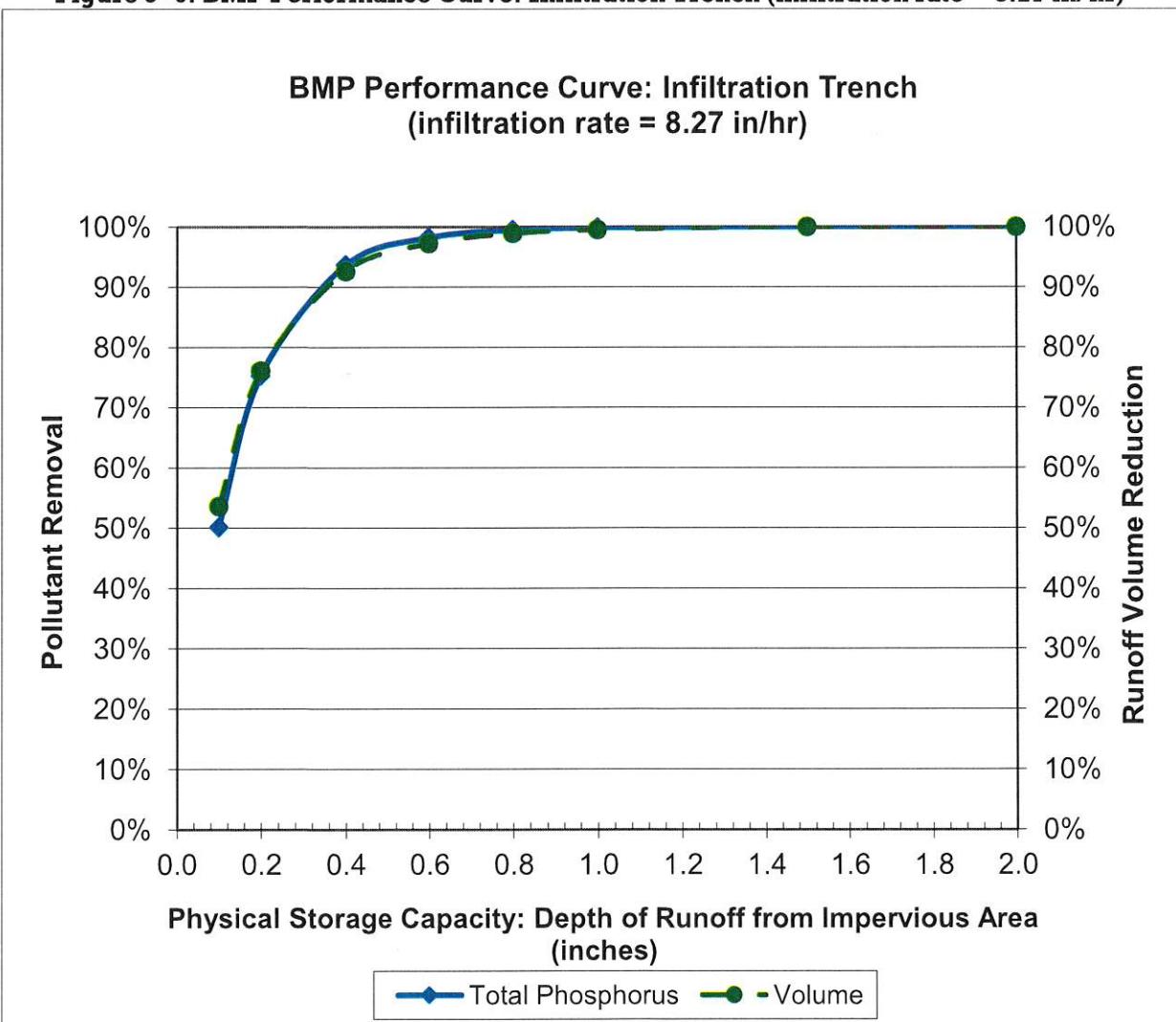
* Lawn/landscaped areas includes all areas included in the HydroCAD calculations (75,400 s.f.) plus an estimated 12,000 s.f. representing the wooded area where the septic system leaching areas will be installed. It should be noted that this Percentage of Reduction is a reduction of the post developed site without BMPs versus with the BMPs.

Appendix F Attachment 3

Table 3- 9: Infiltration Trench (8.27 in/hr) BMP Performance Table

Infiltration Trench (8.27 in/hr) BMP Performance Table: Long-Term Phosphorus Load Reduction								
BMP Capacity: Depth of Runoff Treated from Impervious Area (inches)	0.1	0.2	0.4	0.6	0.8	1.0	1.5	2.0
Runoff Volume Reduction	53.6%	76.1%	92.6%	97.2%	98.9%	99.5%	100.0%	100.0%
Cumulative Phosphorus Load Reduction	50%	75%	94%	98%	99%	100%	100%	100%

Figure 3- 6: BMP Performance Curve: Infiltration Trench (infiltration rate = 8.27 in/hr)



Flow Chart 3: Method to determine the design storage volume of a BMP to reach a known P load reduction when both impervious and pervious drainage areas are present.

- 1) Determine the desired cumulative phosphorus load reduction target (P_{target}) in percentage for the structural BMP;
- 2) Characterize the contributing drainage area to the structural BMP by identifying the following information for the impervious and pervious surfaces:
Impervious area (IA) - Area (acre) and land use (e.g., commercial)

Pervious area (PA) – Area (acre) and runoff depths based on hydrologic soil group (HSG) and rainfall depth. Table 3-3 provides values of runoff depth from pervious areas for various rainfall depths and HSGs. Soils are assigned to an HSG on the basis of their permeability. HSG A is the most permeable, and HSG D is the least permeable. HSG categories for pervious areas in the drainage area shall be estimated by consulting local soil surveys prepared by the National Resource Conservation Service (NRCS) or by a storm water professional evaluating soil testing results from the drainage area. If the HSG condition is not known, a HSG D soil condition should be assumed.

Table 3- 3: Developed Land Pervious Area Runoff Depths based on Precipitation depth and Hydrological Soil Groups (HSGs)

Rainfall Depth, Inches	Runoff Depth, inches				
	Pervious HSG A	Pervious HSG B	Pervious HSG C	Pervious HSG C/D	Pervious HSG D
0.10	0.00	0.00	0.00	0.00	0.00
0.20	0.00	0.00	0.01	0.02	0.02
0.40	0.00	0.00	0.03	0.05	0.06
0.50	0.00	0.01	0.05	0.07	0.09
0.60	0.01	0.02	0.06	0.09	0.11
0.80	0.02	0.03	0.09	0.13	0.16
1.00	0.03	0.04	0.12	0.17	0.21
1.20	0.04	0.05	0.14	0.27	0.39
1.50	0.08	0.11	0.39	0.55	0.72
2.00	0.14	0.22	0.69	0.89	1.08

Notes: Runoff depths derived from combination of volumetric runoff coefficients from Table 5 of *Small Storm Hydrology and Why it is Important for the Design of Stormwater Control Practices*, (Pitt, 1999), and using the Stormwater Management Model (SWMM) in continuous model mode for hourly precipitation data for Boston, MA, 1998-2002.

- 3) Determine the structural BMP type (e.g., infiltration trench, gravel wetland). For infiltration systems, determine the appropriate infiltration rate for the location of the BMP in the Watershed;
- 4) Using the cumulative phosphorus removal performance curve for the selected structural BMP, determine the storage volume capacity of the BMP in inches needed to treat runoff from the contributing impervious area (BMP-Volume $_{IA-in}$);

Appendix F Attachment 3

Table 3- 15: Infiltration Basin (8.27 in/hr) BMP Performance Table

Infiltration Basin (8.27 in/hr) BMP Performance Table: Long-Term Phosphorus Load Reduction								
BMP Capacity: Depth of Runoff Treated from Impervious Area (inches)	0.1	0.2	0.4	0.6	0.8	1.0	1.5	2.0
Runoff Volume Reduction	54.6%	77.2%	93.4%	97.5%	99.0%	99.6%	100.0%	100.0%
Cumulative Phosphorus Load Reduction	59%	81%	96%	99%	100%	100%	100%	100%

Figure 3- 12: BMP Performance Curve: Infiltration Basin (infiltration rate = 8.27 in/hr)

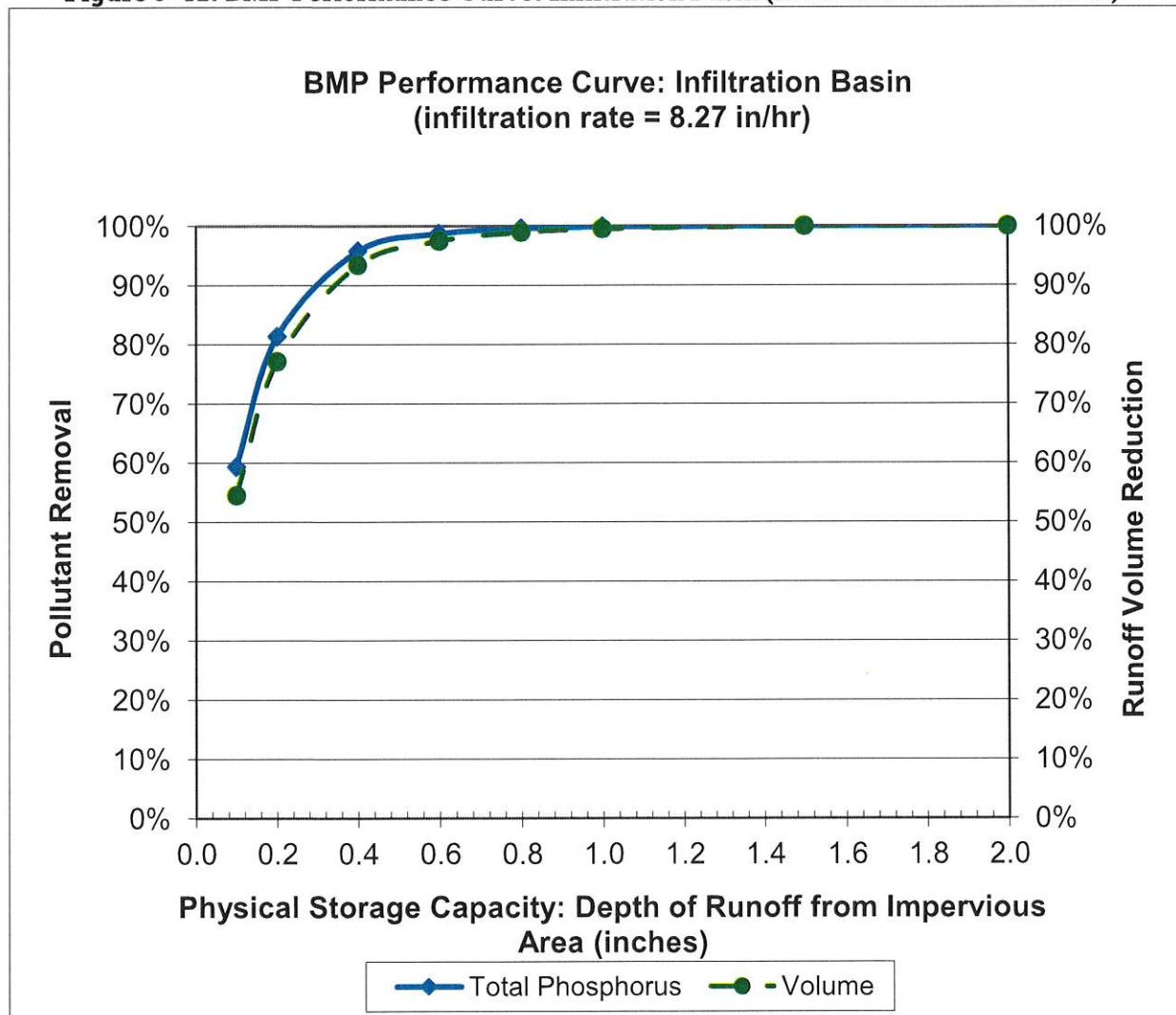


Table 3- 16: Biofiltration BMP Performance Table

Biofiltration BMP Performance Table: Long-Term Phosphorus Load Reduction								
BMP Capacity: Depth of Runoff Treated from Impervious Area (inches)	0.1	0.2	0.4	0.6	0.8	1.0	1.5	2.0
Cumulative Phosphorus Load Reduction	19%	34%	53%	64%	71%	76%	84%	89%

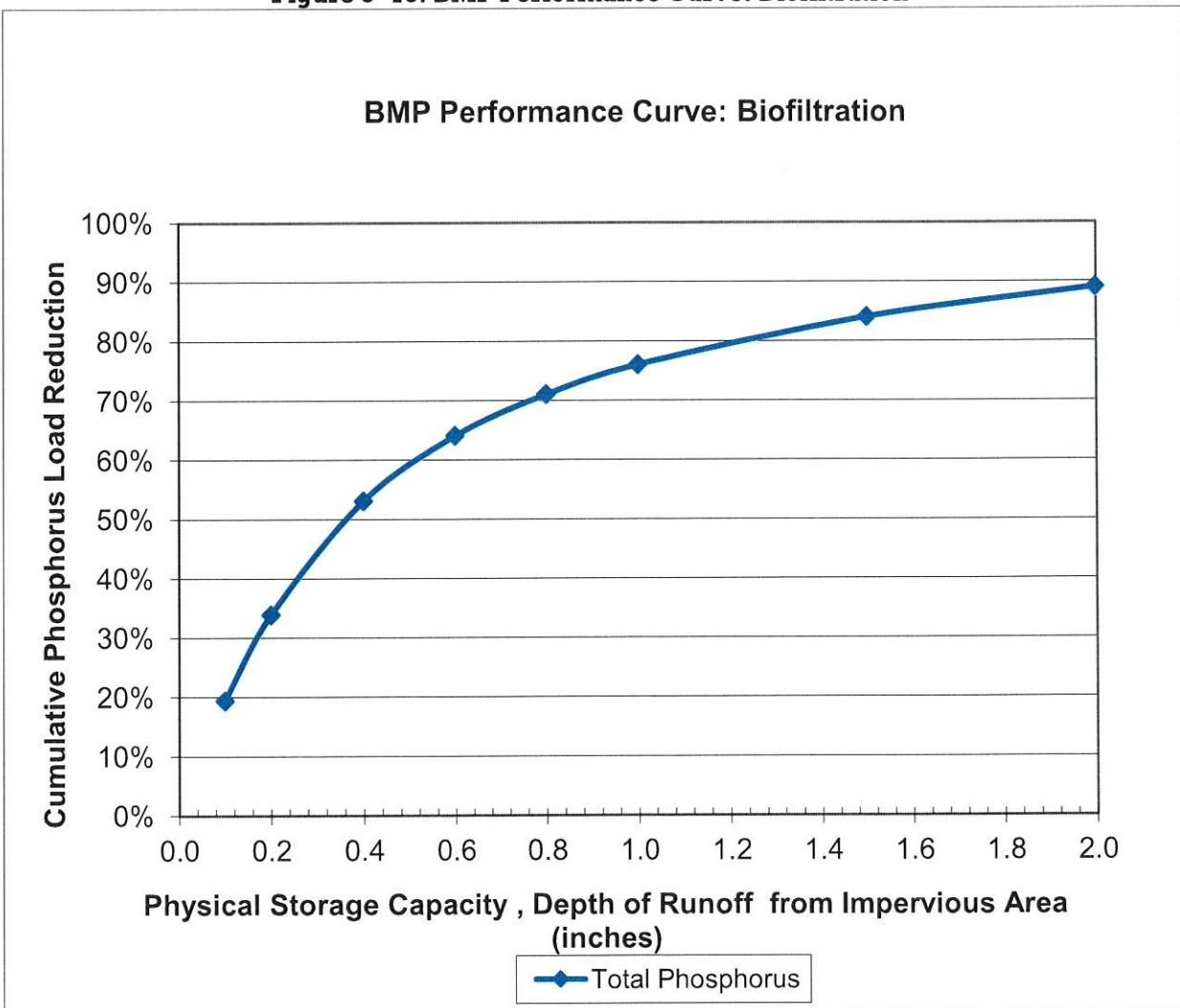
Figure 3- 13: BMP Performance Curve: Biofiltration

Table 3-30 Method for determining stormwater control design volume (DSV) (i.e., capacity) using Long-term cumulative performance curves

Stormwater Control Type	Description	Applicable Structural Stormwater Control Performance Curve	Equation for calculating Design Storage Capacity for Estimating Cumulative Reductions using Performances Curves
Infiltration Trench	Provides temporary storage of runoff using the void spaces within the soil/sand/gravel mixture that is used to backfill the trench for subsequent infiltration into the surrounding sub-soils.	Infiltration Trench (6 infiltration rates: 0.17, 0.27, 0.52, 1.02, 2.41 and 8.27 inches per hour)	DSV = void space volumes of gravel and sand layers DSV = $(L \times W \times D_{soil} \times n_{soil}) + (L \times W \times D_{sand} \times n_{sand})$
Subsurface Infiltration	Provides temporary storage of runoff using the combination of storage structures (e.g., galleries, chambers, pipes, etc.) and void spaces within the soil/sand/gravel mixture that is used to backfill the system for subsequent infiltration into the surrounding sub-soils.	Infiltration Trench (6 infiltration rates: 0.17, 0.27, 0.52, 1.02, 2.41 and 8.27 inches per hour)	DSV = Water storage volume of storage units and void space volumes of backfill materials. Example for subsurface galleries backfilled with washed stone: DSV = $(L \times W \times D_{alley}) + (L \times W \times D_{base} \times n_{base})$
Surface Infiltration	Provides temporary storage of runoff through surface ponding storage structures (e.g., basin or swale) for subsequent infiltration into the underlying soils.	Infiltration Basin (6 infiltration rates: 0.17, 0.27, 0.52, 1.02, 2.41 and 8.27 inches per hour)	DSV = Water volume of storage structure before bypass. DSV = $(L \times W \times D_{alley}) + (L \times W \times D_{base} \times n_{base})$
Rain Garden/Bio-retention (no underdrains)	Provides temporary storage of runoff through surface ponding and possibly void spaces within the soil/sand/gravel mixture that is used to filter runoff prior to infiltration into underlying soils.	Infiltration Basin (6 infiltration rates: 0.17, 0.27, 0.52, 1.02, 2.41 and 8.27 inches per hour)	DSV = Ponding water storage volume and void space volumes of soil filter media. Example for raingarden: DSV = $(A_{pond} \times D_{pond}) + (A_{soil} \times D_{soil} \times n_{soil_mix})$
Tree Filter (no underdrain)	Provides temporary storage of runoff through surface ponding and void spaces within the soil/sand/gravel mixture that is used to filter runoff prior to infiltration into underlying soils.	Infiltration Trench (6 infiltration rates: 0.17, 0.27, 0.52, 1.02, 2.41 and 8.27 inches per hour)	DSV = Ponding water storage volume and void space volumes of soil filter media. Example for a linear biofilter: DSV = $(L \times W \times D_{pond}) + (L \times W \times D_{soil} \times n_{soil_mix})$
Bio-Filtration (w/underdrain)	Provides temporary storage of runoff for filtering through an engineered soil media. The storage capacity includes void spaces in the filter media and temporary ponding at the surface. After runoff has passed through the filter media it is collected by an under-drain pipe for discharge. Manufactured or packaged bio-filter systems such as tree box filters may be suitable for using the bio-filtration performance results.	Bio-filtration	DSV = Ponding water storage volume and void space volume of soil filter media. Example of a linear biofilter: DSV = $(L \times W \times D_{pond}) + (L \times W \times D_{soil} \times n_{soil})$
Gravel Wetland	Based on design by the UNH Stormwater Center (UNHSC). Provides temporary surface ponding storage of runoff in a vegetated wetland cell that is eventually routed to an underlying saturated gravel internal storage reservoir (ISR) for nitrogen treatment. Outflow is controlled by an elevated orifice that has an invert elevation equal to the top of the ISR layer and provides a retention time of at least 24 hours.	Gravel Wetland	DSV = pretreatment volume + ponding volume + void space volume of gravel ISR. DSV = $(A_{pretreatment} \times D_{pretreatment}) + (A_{wetland} \times D_{ponding}) + (A_{ISR} \times D_{gavel} \times n_{gavel})$
Porous Pavement w/ subsurface infiltration	Provides filtering of runoff through a filter course and temporary storage of runoff within the void spaces of a subsurface gravel reservoir prior to infiltration into subsoils.	Infiltration Trench (6 infiltration rates: 0.17, 0.27, 0.52, 1.02, 2.41 and 8.27 inches per hour)	DSV = void space volumes of gravel layer. DSV = $(L \times W \times D_{soil} \times n_{soil})$
Porous pavement w/ impermeable underliner w/underdrain	Provides filtering of runoff through a filter course and temporary storage of runoff within the void spaces prior to discharge by way of an underdrain.	Porous Pavement	Depth of Filter Course = D _{FC}
Wet Pond	Provides treatment of runoff through routing through permanent pool.	Wet Pond	DSV = Permanent pool volume prior to high flow bypass DSV = $A_{pond} \times D_{pond}$ (does not include pre-treatment volume)
Extended Dry Detention Basin	Provides temporary detention storage for the design storage volume to drain in 24 hours through multiple out let controls.	Dry Pond	DSV = Ponding volume prior to high flow bypass DSV = $A_{pond} \times D_{pond}$ (does not include pre-treatment volume)
Dry Water Quality Swale/Grass Swale	Based on MA design standards. Provides temporary surface ponding storage of runoff in an open vegetated channel through permeable check dams. Treatment is provided by filtering of runoff by vegetation and check dams and infiltration into subsurface soils.	Grass swale	DSV = Volume of swale at full design depth DSV = $L_{swale} \times A_{swale}$

Definitions: **DSV**= Design Storage Volume = physical storage capacity to hold water; **VSV** = Void Space Volume; **L** = length, **W** = width, **D** = depth at design capacity before bypass, **n** = porosity fill material, **A**= average surface area for calculating volume; **Infiltration rate** = saturated soil hydraulic conductivity

Supporting Data – CDS TSS Removal Calculations

Hydrodynamic Separation Product Calculator

Littleton Warehouse 1

Stormwater Treatment Unit 1

CDS 2015-4

Project Information

Project Name	Littleton Warehouse 1			Option #	A
Country	UNITED STATES	State	Massachusetts	City	Littleton

Contact Information

First Name	Patrick	Last Name	Burke
Company	Places Associates, Inc.	Phone #	978-486-0334
Email	pburke@placesassociates.com		

Design Criteria

Site Designation	Stormwater Treatment Unit 1			Sizing Method	Net Annual
Screening Required?	No	Drainage Area (ac)	0.60	Peak Flow (cfs)	3.59
Groundwater Depth (ft)	5 - 10	Pipe Invert Depth (ft)	0 - 5	Bedrock Depth (ft)	>15
Multiple Inlets?	No	Grate Inlet Required?	No	Pipe Size (in)	12.00
Required Particle Size Distribution?	No	90° between two inlets?	N/A	180° between inlet and outlet?	No
Runoff Coefficient	0.81	Rainfall Station	71 - Birch Hill Dam, MA	TC (Min)	6

Treatment Selection

Treatment Unit	CDS	System Model	2015-4		
Target Removal	80%	Particle Size Distribution (PSD)	125	Predicted Net Annual Removal	96.09%

Hydrodynamic Separation Product Calculator

Littleton Warehouse 1

Stormwater Treatment Unit 1

CDS 2015-4

CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION BASED ON THE RATIONAL RAINFALL METHOD

Rainfall Intensity ¹ (in/hr)	% Rainfall Volume ¹	Cumulative Rainfall Volume	Rainfall Volume Treated	Total Flowrate (cfs)	Treated Flowrate (cfs)	Operating Rate (%)	Removal Efficiency (%)	Incremental Removal (%)
0.0800	37.59%	37.59%	37.59%	0.0389	0.0389	5.56%	100.00%	37.59%
0.1600	22.64%	60.23%	22.64%	0.0778	0.0778	11.11%	99.19%	22.46%
0.2400	11.89%	72.12%	11.89%	0.1166	0.1166	16.66%	98.08%	11.66%
0.3200	7.58%	79.70%	7.58%	0.1555	0.1555	22.21%	96.97%	7.35%
0.4000	4.35%	84.05%	4.35%	0.1944	0.1944	27.77%	95.85%	4.17%
0.4800	2.35%	86.40%	2.35%	0.2333	0.2333	33.33%	94.74%	2.23%
0.5600	1.79%	88.19%	1.79%	0.2722	0.2722	38.89%	93.63%	1.68%
0.6400	1.37%	89.56%	1.37%	0.3110	0.3110	44.43%	92.52%	1.27%
0.7200	0.87%	90.43%	0.87%	0.3499	0.3499	49.99%	91.41%	0.80%
0.8000	1.16%	91.59%	1.16%	0.3888	0.3888	55.54%	90.30%	1.05%
0.8800	1.49%	93.08%	1.49%	0.4277	0.4277	61.10%	89.18%	1.33%
0.9600	0.93%	94.01%	0.93%	0.4666	0.4666	66.66%	88.07%	0.82%
1.0400	0.38%	94.39%	0.38%	0.5054	0.5054	72.20%	86.96%	0.33%
1.1200	0.41%	94.80%	0.41%	0.5443	0.5443	77.76%	85.85%	0.35%
1.2000	0.58%	95.38%	0.58%	0.5832	0.5832	83.31%	84.74%	0.49%
1.2800	0.31%	95.69%	0.31%	0.6221	0.6221	88.87%	83.63%	0.26%
1.3600	0.17%	95.86%	0.17%	0.6610	0.6610	94.43%	82.51%	0.14%
1.4400	0.88%	96.74%	0.88%	0.6998	0.6998	99.97%	81.41%	0.72%
1.5200	0.55%	97.29%	0.52%	0.7387	0.7000	100.00%	77.14%	0.42%
1.6000	0.40%	97.69%	0.36%	0.7776	0.7000	100.00%	73.28%	0.29%
1.8000	0.20%	97.89%	0.16%	0.8748	0.7000	100.00%	65.13%	0.13%
2.0000	0.94%	98.83%	0.68%	0.9720	0.7000	100.00%	58.62%	0.55%
								96.09%
Removal Efficiency Adjustment ² =								
Predicted % Annual Rainfall Treated =								98.46%
Predicted Net Annual Load Removal Efficiency =								96.09%

1 - Based on 13 years of 15 minute precipitation data for Station 0666, Birch Hill Dam, Worcester County, MA

2 - Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.

Hydrodynamic Separation Product Calculator

Littleton Warehouse 1

Stormwater Treatment Unit 2

CDS 2015-4

Project Information

Project Name	Littleton Warehouse 1			Option #	A
Country	UNITED STATES	State	Massachusetts	City	Littleton

Contact Information

First Name	Patrick	Last Name	Burke
Company	Places Associates, Inc.	Phone #	978-486-0334
Email	pburke@placesassociates.com		

Design Criteria

Site Designation	Stormwater Treatment Unit 2			Sizing Method	Net Annual
Screening Required?	No	Drainage Area (ac)	0.43	Peak Flow (cfs)	3.19
Groundwater Depth (ft)	5 - 10	Pipe Invert Depth (ft)	5 - 10	Bedrock Depth (ft)	>15
Multiple Inlets?	No	Grate Inlet Required?	Yes	Pipe Size (in)	12.00
Required Particle Size Distribution?	No	90° between two inlets?	N/A	180° between inlet and outlet?	No
Runoff Coefficient	0.90	Rainfall Station	71 - Birch Hill Dam, MA	TC (Min)	6

Treatment Selection

Treatment Unit	CDS	System Model	2015-4		
Target Removal	80%	Particle Size Distribution (PSD)	125	Predicted Net Annual Removal	96.90%

Hydrodynamic Separation Product Calculator

Littleton Warehouse 1

Stormwater Treatment Unit 2

CDS 2015-4

CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION BASED ON THE RATIONAL RAINFALL METHOD

Rainfall Intensity ¹ (in/hr)	% Rainfall Volume ¹	Cumulative Rainfall Volume	Rainfall Volume Treated	Total Flowrate (cfs)	Treated Flowrate (cfs)	Operating Rate (%)	Removal Efficiency (%)	Incremental Removal (%)
0.0800	37.59%	37.59%	37.59%	0.0310	0.0310	4.43%	100.00%	37.59%
0.1600	22.64%	60.23%	22.64%	0.0619	0.0619	8.84%	99.64%	22.56%
0.2400	11.89%	72.12%	11.89%	0.0929	0.0929	13.27%	98.75%	11.74%
0.3200	7.58%	79.70%	7.58%	0.1238	0.1238	17.69%	97.87%	7.42%
0.4000	4.35%	84.05%	4.35%	0.1548	0.1548	22.11%	96.99%	4.22%
0.4800	2.35%	86.40%	2.35%	0.1858	0.1858	26.54%	96.10%	2.26%
0.5600	1.79%	88.19%	1.79%	0.2167	0.2167	30.96%	95.21%	1.70%
0.6400	1.37%	89.56%	1.37%	0.2477	0.2477	35.39%	94.33%	1.29%
0.7200	0.87%	90.43%	0.87%	0.2786	0.2786	39.80%	93.45%	0.81%
0.8000	1.16%	91.59%	1.16%	0.3096	0.3096	44.23%	92.56%	1.07%
0.8800	1.49%	93.08%	1.49%	0.3406	0.3406	48.66%	91.67%	1.37%
0.9600	0.93%	94.01%	0.93%	0.3715	0.3715	53.07%	90.79%	0.84%
1.0400	0.38%	94.39%	0.38%	0.4025	0.4025	57.50%	89.90%	0.34%
1.1200	0.41%	94.80%	0.41%	0.4334	0.4334	61.91%	89.02%	0.36%
1.2000	0.58%	95.38%	0.58%	0.4644	0.4644	66.34%	88.14%	0.51%
1.2800	0.31%	95.69%	0.31%	0.4954	0.4954	70.77%	87.25%	0.27%
1.3600	0.17%	95.86%	0.17%	0.5263	0.5263	75.19%	86.36%	0.15%
1.4400	0.88%	96.74%	0.88%	0.5573	0.5573	79.61%	85.48%	0.75%
1.5200	0.55%	97.29%	0.55%	0.5882	0.5882	84.03%	84.60%	0.47%
1.6000	0.40%	97.69%	0.40%	0.6192	0.6192	88.46%	83.71%	0.33%
1.8000	0.20%	97.89%	0.20%	0.6966	0.6966	99.51%	81.50%	0.16%
2.0000	0.94%	98.83%	0.85%	0.7740	0.7000	100.00%	73.62%	0.69%
								96.90%
								Removal Efficiency Adjustment ² =
								Predicted % Annual Rainfall Treated =
								Predicted Net Annual Load Removal Efficiency =

1 - Based on 13 years of 15 minute precipitation data for Station 0666, Birch Hill Dam, Worcester County, MA

2 - Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.

Hydrodynamic Separation Product Calculator

Littleton Warehouse 1

Stormwater Treatment Unit 3

CDS 2015-4

Project Information

Project Name	Littleton Warehouse 1			Option #	A
Country	UNITED STATES	State	Massachusetts	City	Littleton

Contact Information

First Name	Patrick	Last Name	Burke
Company	Places Associates, Inc.	Phone #	978-486-0334
Email	pburke@placesassociates.com		

Design Criteria

Site Designation	Stormwater Treatment Unit 3			Sizing Method	Net Annual
Screening Required?	No	Drainage Area (ac)	0.16	Peak Flow (cfs)	1.14
Groundwater Depth (ft)	5 - 10	Pipe Invert Depth (ft)	0 - 5	Bedrock Depth (ft)	>15
Multiple Inlets?	No	Grate Inlet Required?	No	Pipe Size (in)	12.00
Required Particle Size Distribution?	No	90° between two inlets?	N/A	180° between inlet and outlet?	No
Runoff Coefficient	0.90	Rainfall Station	71 - Birch Hill Dam, MA	TC (Min)	6

Treatment Selection

Treatment Unit	CDS	System Model	2015-4		
Target Removal	80%	Particle Size Distribution (PSD)	125	Predicted Net Annual Removal	98.47%

Hydrodynamic Separation Product Calculator

Littleton Warehouse 1

Stormwater Treatment Unit 3

CDS 2015-4

CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION BASED ON THE RATIONAL RAINFALL METHOD

Rainfall Intensity ¹ (in/hr)	% Rainfall Volume ¹	Cumulative Rainfall Volume	Rainfall Volume Treated	Total Flowrate (cfs)	Treated Flowrate (cfs)	Operating Rate (%)	Removal Efficiency (%)	Incremental Removal (%)
0.0800	37.59%	37.59%	37.59%	0.0115	0.0115	1.64%	100.00%	37.59%
0.1600	22.64%	60.23%	22.64%	0.0230	0.0230	3.29%	100.00%	22.64%
0.2400	11.89%	72.12%	11.89%	0.0346	0.0346	4.94%	100.00%	11.89%
0.3200	7.58%	79.70%	7.58%	0.0461	0.0461	6.59%	100.00%	7.58%
0.4000	4.35%	84.05%	4.35%	0.0576	0.0576	8.23%	99.76%	4.34%
0.4800	2.35%	86.40%	2.35%	0.0691	0.0691	9.87%	99.44%	2.34%
0.5600	1.79%	88.19%	1.79%	0.0806	0.0806	11.51%	99.11%	1.77%
0.6400	1.37%	89.56%	1.37%	0.0922	0.0922	13.17%	98.77%	1.35%
0.7200	0.87%	90.43%	0.87%	0.1037	0.1037	14.81%	98.45%	0.86%
0.8000	1.16%	91.59%	1.16%	0.1152	0.1152	16.46%	98.12%	1.14%
0.8800	1.49%	93.08%	1.49%	0.1267	0.1267	18.10%	97.79%	1.46%
0.9600	0.93%	94.01%	0.93%	0.1382	0.1382	19.74%	97.46%	0.91%
1.0400	0.38%	94.39%	0.38%	0.1498	0.1498	21.40%	97.13%	0.37%
1.1200	0.41%	94.80%	0.41%	0.1613	0.1613	23.04%	96.80%	0.40%
1.2000	0.58%	95.38%	0.58%	0.1728	0.1728	24.69%	96.47%	0.56%
1.2800	0.31%	95.69%	0.31%	0.1843	0.1843	26.33%	96.14%	0.30%
1.3600	0.17%	95.86%	0.17%	0.1958	0.1958	27.97%	95.81%	0.16%
1.4400	0.88%	96.74%	0.88%	0.2074	0.2074	29.63%	95.48%	0.84%
1.5200	0.55%	97.29%	0.55%	0.2189	0.2189	31.27%	95.15%	0.52%
1.6000	0.40%	97.69%	0.40%	0.2304	0.2304	32.91%	94.82%	0.38%
1.8000	0.20%	97.89%	0.20%	0.2592	0.2592	37.03%	94.00%	0.19%
2.0000	0.94%	98.83%	0.94%	0.2880	0.2880	41.14%	93.18%	0.88%
								98.47%
Removal Efficiency Adjustment ² =								
Predicted % Annual Rainfall Treated =								98.83%
Predicted Net Annual Load Removal Efficiency =								98.47%

1 - Based on 13 years of 15 minute precipitation data for Station 0666, Birch Hill Dam, Worcester County, MA

2 - Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.

MADEP Stormwater Checklist



Checklist for Stormwater Report

B. Stormwater Checklist and Certification

The following checklist is intended to serve as a guide for applicants as to the elements that ordinarily need to be addressed in a complete Stormwater Report. The checklist is also intended to provide conservation commissions and other reviewing authorities with a summary of the components necessary for a comprehensive Stormwater Report that addresses the ten Stormwater Standards.

Note: Because stormwater requirements vary from project to project, it is possible that a complete Stormwater Report may not include information on some of the subjects specified in the Checklist. If it is determined that a specific item does not apply to the project under review, please note that the item is not applicable (N.A.) and provide the reasons for that determination.

A complete checklist must include the Certification set forth below signed by the Registered Professional Engineer who prepared the Stormwater Report.

Registered Professional Engineer's Certification

I have reviewed the Stormwater Report, including the soil evaluation, computations, Long-term Pollution Prevention Plan, the Construction Period Erosion and Sedimentation Control Plan (if included), the Long-term Post-Construction Operation and Maintenance Plan, the Illicit Discharge Compliance Statement (if included) and the plans showing the stormwater management system, and have determined that they have been prepared in accordance with the requirements of the Stormwater Management Standards as further elaborated by the Massachusetts Stormwater Handbook. I have also determined that the information presented in the Stormwater Checklist is accurate and that the information presented in the Stormwater Report accurately reflects conditions at the site as of the date of this permit application.

Registered Professional Engineer Block and Signature



Signature and Date

Susan Carter 6/27/22

Checklist

Project Type: Is the application for new development, redevelopment, or a mix of new and redevelopment?

- New development
- Redevelopment
- Mix of New Development and Redevelopment



Checklist for Stormwater Report

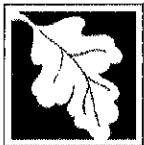
Checklist (continued)

LID Measures: Stormwater Standards require LID measures to be considered. Document what environmentally sensitive design and LID Techniques were considered during the planning and design of the project:

- No disturbance to any Wetland Resource Areas
- Site Design Practices (e.g. clustered development, reduced frontage setbacks)
- Reduced Impervious Area (Redevelopment Only)
- Minimizing disturbance to existing trees and shrubs
- LID Site Design Credit Requested:
 - Credit 1
 - Credit 2
 - Credit 3
- Use of "country drainage" versus curb and gutter conveyance and pipe
- Bioretention Cells (includes Rain Gardens)
- Constructed Stormwater Wetlands (includes Gravel Wetlands designs)
- Treebox Filter
- Water Quality Swale
- Grass Channel
- Green Roof
- Other (describe): _____

Standard 1: No New Untreated Discharges

- No new untreated discharges
- Outlets have been designed so there is no erosion or scour to wetlands and waters of the Commonwealth
- Supporting calculations specified in Volume 3 of the Massachusetts Stormwater Handbook included.



Checklist for Stormwater Report

Checklist (continued)

Standard 2: Peak Rate Attenuation

- Standard 2 waiver requested because the project is located in land subject to coastal storm flowage and stormwater discharge is to a wetland subject to coastal flooding.
- Evaluation provided to determine whether off-site flooding increases during the 100-year 24-hour storm.
- Calculations provided to show that post-development peak discharge rates do not exceed pre-development rates for the 2-year and 10-year 24-hour storms. If evaluation shows that off-site flooding increases during the 100-year 24-hour storm, calculations are also provided to show that post-development peak discharge rates do not exceed pre-development rates for the 100-year 24-hour storm.

Standard 3: Recharge

- Soil Analysis provided.
- Required Recharge Volume calculation provided.
- Required Recharge volume reduced through use of the LID site Design Credits.
- Sizing the infiltration, BMPs is based on the following method: Check the method used.
 - Static
 - Simple Dynamic
 - Dynamic Field¹
- Runoff from all impervious areas at the site discharging to the infiltration BMP.
- Runoff from all impervious areas at the site is *not* discharging to the infiltration BMP and calculations are provided showing that the drainage area contributing runoff to the infiltration BMPs is sufficient to generate the required recharge volume.
- Recharge BMPs have been sized to infiltrate the Required Recharge Volume.
- Recharge BMPs have been sized to infiltrate the Required Recharge Volume *only* to the maximum extent practicable for the following reason:
 - Site is comprised solely of C and D soils and/or bedrock at the land surface
 - M.G.L. c. 21E sites pursuant to 310 CMR 40.0000
 - Solid Waste Landfill pursuant to 310 CMR 19.000
 - Project is otherwise subject to Stormwater Management Standards only to the maximum extent practicable.
- Calculations showing that the infiltration BMPs will drain in 72 hours are provided.
- Property includes a M.G.L. c. 21E site or a solid waste landfill and a mounding analysis is included.

¹ 80% TSS removal is required prior to discharge to infiltration BMP if Dynamic Field method is used.



Checklist for Stormwater Report

Checklist (continued)

Standard 3: Recharge (continued)

- The infiltration BMP is used to attenuate peak flows during storms greater than or equal to the 10-year 24-hour storm and separation to seasonal high groundwater is less than 4 feet and a mounding analysis is provided.
- Documentation is provided showing that infiltration BMPs do not adversely impact nearby wetland resource areas.

Standard 4: Water Quality

The Long-Term Pollution Prevention Plan typically includes the following:

- Good housekeeping practices;
- Provisions for storing materials and waste products inside or under cover;
- Vehicle washing controls;
- Requirements for routine inspections and maintenance of stormwater BMPs;
- Spill prevention and response plans;
- Provisions for maintenance of lawns, gardens, and other landscaped areas;
- Requirements for storage and use of fertilizers, herbicides, and pesticides;
- Pet waste management provisions;
- Provisions for operation and management of septic systems;
- Provisions for solid waste management;
- Snow disposal and plowing plans relative to Wetland Resource Areas;
- Winter Road Salt and/or Sand Use and Storage restrictions;
- Street sweeping schedules;
- Provisions for prevention of illicit discharges to the stormwater management system;
- Documentation that Stormwater BMPs are designed to provide for shutdown and containment in the event of a spill or discharges to or near critical areas or from LUHPPL;
- Training for staff or personnel involved with implementing Long-Term Pollution Prevention Plan;
- List of Emergency contacts for implementing Long-Term Pollution Prevention Plan.

- A Long-Term Pollution Prevention Plan is attached to Stormwater Report and is included as an attachment to the Wetlands Notice of Intent.
- Treatment BMPs subject to the 44% TSS removal pretreatment requirement and the one inch rule for calculating the water quality volume are included, and discharge:
 - is within the Zone II or Interim Wellhead Protection Area
 - is near or to other critical areas
 - is within soils with a rapid infiltration rate (greater than 2.4 inches per hour)
 - involves runoff from land uses with higher potential pollutant loads.
- The Required Water Quality Volume is reduced through use of the LID site Design Credits.
- Calculations documenting that the treatment train meets the 80% TSS removal requirement and, if applicable, the 44% TSS removal pretreatment requirement, are provided.



Checklist for Stormwater Report

Checklist (continued)

Standard 4: Water Quality (continued)

- The BMP is sized (and calculations provided) based on:
 - The $\frac{1}{2}$ " or 1" Water Quality Volume or
 - The equivalent flow rate associated with the Water Quality Volume and documentation is provided showing that the BMP treats the required water quality volume.
- The applicant proposes to use proprietary BMPs, and documentation supporting use of proprietary BMP and proposed TSS removal rate is provided. This documentation may be in the form of the proprietary BMP checklist found in Volume 2, Chapter 4 of the Massachusetts Stormwater Handbook and submitting copies of the TARP Report, STEP Report, and/or other third party studies verifying performance of the proprietary BMPs.
- A TMDL exists that indicates a need to reduce pollutants other than TSS and documentation showing that the BMPs selected are consistent with the TMDL is provided.

Standard 5: Land Uses With Higher Potential Pollutant Loads (LUHPPLs)

- The NPDES Multi-Sector General Permit covers the land use and the Stormwater Pollution Prevention Plan (SWPPP) has been included with the Stormwater Report.
- The NPDES Multi-Sector General Permit covers the land use and the SWPPP will be submitted *prior to* the discharge of stormwater to the post-construction stormwater BMPs.
- The NPDES Multi-Sector General Permit does *not* cover the land use.
- LUHPPLs are located at the site and industry specific source control and pollution prevention measures have been proposed to reduce or eliminate the exposure of LUHPPLs to rain, snow, snow melt and runoff, and been included in the long term Pollution Prevention Plan.
- All exposure has been eliminated.
- All exposure has *not* been eliminated and all BMPs selected are on MassDEP LUHPPL list.
- The LUHPPL has the potential to generate runoff with moderate to higher concentrations of oil and grease (e.g. all parking lots with >1000 vehicle trips per day) and the treatment train includes an oil grit separator, a filtering bioretention area, a sand filter or equivalent.

Standard 6: Critical Areas

- The discharge is near or to a critical area and the treatment train includes only BMPs that MassDEP has approved for stormwater discharges to or near that particular class of critical area.
- Critical areas and BMPs are identified in the Stormwater Report.



Checklist for Stormwater Report

Checklist (continued)

Standard 7: Redevelopments and Other Projects Subject to the Standards only to the maximum extent practicable

The project is subject to the Stormwater Management Standards only to the maximum Extent Practicable as a:

- Limited Project
- Small Residential Projects: 5-9 single family houses or 5-9 units in a multi-family development provided there is no discharge that may potentially affect a critical area.
- Small Residential Projects: 2-4 single family houses or 2-4 units in a multi-family development with a discharge to a critical area
- Marina and/or boatyard provided the hull painting, service and maintenance areas are protected from exposure to rain, snow, snow melt and runoff
- Bike Path and/or Foot Path
- Redevelopment Project
- Redevelopment portion of mix of new and redevelopment.

Certain standards are not fully met (Standard No. 1, 8, 9, and 10 must always be fully met) and an explanation of why these standards are not met is contained in the Stormwater Report.

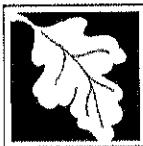
The project involves redevelopment and a description of all measures that have been taken to improve existing conditions is provided in the Stormwater Report. The redevelopment checklist found in Volume 2 Chapter 3 of the Massachusetts Stormwater Handbook may be used to document that the proposed stormwater management system (a) complies with Standards 2, 3 and the pretreatment and structural BMP requirements of Standards 4-6 to the maximum extent practicable and (b) improves existing conditions.

Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan must include the following information:

- Narrative;
- Construction Period Operation and Maintenance Plan;
- Names of Persons or Entity Responsible for Plan Compliance;
- Construction Period Pollution Prevention Measures;
- Erosion and Sedimentation Control Plan Drawings;
- Detail drawings and specifications for erosion control BMPs, including sizing calculations;
- Vegetation Planning;
- Site Development Plan;
- Construction Sequencing Plan;
- Sequencing of Erosion and Sedimentation Controls;
- Operation and Maintenance of Erosion and Sedimentation Controls;
- Inspection Schedule;
- Maintenance Schedule;
- Inspection and Maintenance Log Form.

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan containing the information set forth above has been included in the Stormwater Report.



Checklist for Stormwater Report

Checklist (continued)

Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control (continued)

- The project is highly complex and information is included in the Stormwater Report that explains why it is not possible to submit the Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan with the application. A Construction Period Pollution Prevention and Erosion and Sedimentation Control has **not** been included in the Stormwater Report but will be submitted **before** land disturbance begins.
- The project is **not** covered by a NPDES Construction General Permit.
- The project is covered by a NPDES Construction General Permit and a copy of the SWPPP is in the Stormwater Report.
- The project is covered by a NPDES Construction General Permit but no SWPPP been submitted. The SWPPP will be submitted BEFORE land disturbance begins.

Standard 9: Operation and Maintenance Plan

- The Post Construction Operation and Maintenance Plan is included in the Stormwater Report and includes the following information:
 - Name of the stormwater management system owners;
 - Party responsible for operation and maintenance;
 - Schedule for implementation of routine and non-routine maintenance tasks;
 - Plan showing the location of all stormwater BMPs maintenance access areas;
 - Description and delineation of public safety features;
 - Estimated operation and maintenance budget; and
 - Operation and Maintenance Log Form.
- The responsible party is **not** the owner of the parcel where the BMP is located and the Stormwater Report includes the following submissions:
 - A copy of the legal instrument (deed, homeowner's association, utility trust or other legal entity) that establishes the terms of and legal responsibility for the operation and maintenance of the project site stormwater BMPs;
 - A plan and easement deed that allows site access for the legal entity to operate and maintain BMP functions.

Standard 10: Prohibition of Illicit Discharges

- The Long-Term Pollution Prevention Plan includes measures to prevent illicit discharges;
- An Illicit Discharge Compliance Statement is attached;
- NO Illicit Discharge Compliance Statement is attached but will be submitted **prior to** the discharge of any stormwater to post-construction BMPs.

Stormwater Operation and Maintenance Plan

Stormwater Operation and Maintenance Plan - Long Term Pollution Prevention

Ongoing maintenance is required for the proper function of the stormwater management system allowing the system prevent pollution for the long term. This document provides a guideline for this work and allows for record keeping.

Stormwater Management System Owner: To be determined

Signature/date

Party Responsible for Maintenance: To be determined

Signature/date

Snow Removal

Snow removal from parking areas will be the responsibility of the property owner.

Public Safety Features

The site has been designed with sidewalks and lighting to allow for safe movement throughout the site.

Preliminary Stormwater O&M Maintenance Budget

Inspection and maintenance = $\$1,250 \times 4$ times per year = $\$5,000 \pm$

Site Specific BMP Maintenance Plans

(Reference MADEP Volume 2, Chapter – Structural BMP Specifications for the Massachusetts Stormwater Handbook)

Routine Maintenance

Routine maintenance of lawns, gardens, and other landscaped areas shall occur as necessary to maintain the property in a neat and orderly fashion. Clippings and/or mulch shall not be washed into the drainage infrastructure.

Catch Basins and Manholes

Regular maintenance is essential. Deep sump catch basins remain effective at removing pollutants only if they are cleaned out frequently. Once 50% of the sump volume is filled, the catch basin may not be able to retain additional sediment.

Inspect or clean deep sumps at least four times per year and at the end of the foliage and snow removal seasons. Sediments must also be removed four times per year or whenever the depth of deposits is greater than or equal to one half the depth from the bottom of the invert of the lowest pipe in the basin. Clamshell buckets are typically used to remove sediment; however, vacuum trucks are preferable as they remove more trapped sediment than clamshells. Vacuuming is also a speedier process and is less likely to damage the hood within the deep sump catch basin.

Trench Drains

Inspect trench drains four times per year. Remove sediments each spring and when accumulation is 3 inches deep. Inspect grates and repair or replace, as necessary.

Infiltration Basins

Inspect and complete preventive maintenance at least twice a year, and after every time drainage discharges through the emergency spillway. Inspect the pretreatment as required. Once the basin is in use, inspect it after every major storm for the first few months to ensure it is stabilized and functioning properly and if necessary, take corrective action. Note how long water remains standing in the basin after a storm; standing water within the basin 48 to 72 hours after a storm indicates the infiltration capacity may have been overestimated. If the ponding is due to clogging, immediately address the reasons for the clogging (such as upland sediment erosion, excessive compaction of soils, or low spots). Thereafter, inspect the infiltration basin at least twice per year. Important items to check during the inspection include:

- Signs of differential settlement
- Cracking, Erosion
- Leakage in the embankments
- Tree growth on the embankments
- Condition of riprap
- Sediment accumulation
- The health of the turf.

At least twice a year, mow the buffer area, side slopes, and basin bottom if grassed. Remove grass clippings and accumulated organic matter to prevent an impervious organic mat from forming. Remove trash and debris at the same time. Use deep tilling to break up clogged surfaces and revegetate immediately. Remove sediment from the basin as necessary but wait until the floor of the basin is thoroughly dry. Use light equipment to remove the top layer to not compact the underlying

soil. Deeply till the remaining soil and revegetate as soon as possible. Inspect and clean pretreatment devices per O&M.

Infiltration Chambers

Follow manufacturer's recommended Inspection and maintenance program. Inspect infiltration chambers at least once per year to ensure that the basins are operating as intended. Inspect infiltration chambers during and after major storms to determine if the chambers are meeting the expected detention times. Examine the outlet structure for evidence of clogging or outflow release velocities that are greater than design flow. Potential problems that should be checked include: subsidence, erosion, cracking, or tree growth on or near the chambers; sediment accumulation around the outlet; inadequacy of the inlet/outlet channel erosion control measures; and erosion or sedimentation at the inlets. Make any necessary repairs immediately. During inspections, note any changes to the infiltration chambers or the contributing watershed, because these could affect chamber performance. Also remove trash and debris at this time. Remove sediment from the in chambers as necessary, but at least once every 5 years. Providing an on-site sediment disposal area will reduce the overall sediment removal costs.

Tree Box Filters

Inspect and complete preventive maintenance quarterly during first year following construction and after every major storm in the first few months. Important items to inspect:

- Check to ensure the filter surface remains well draining after storms. The system should drain completely within 72 hours.
If filter bed is clogged, draining poorly, or standing water covers more than 50% of the surface 48 hours after a precipitation event, remove top few inches of discolored material. Till, or rake remaining material as needed. Replace mulch as necessary.
- Check inlets and outlets for leaves and debris.
Rake in and around the system to clear it of debris. Also, clear the inlet and overflow if obstructed.
- Check for animal burrows and short circuiting the system.
Soil erosion from short circuiting or animal burrows should be repaired when they occur. The holes should be filled and lightly compacted.
- Inspect inlets and outlets to ensure good condition and no evidence of deterioration. Check to see if high-flow bypass is functioning.
Repair or replace any damaged structural parts, inlets, outlets, sidewalls.
- Check health of trees. Tree is stable and roots are not exposed.
- Keep a record of inspections.

Stormwater Treatment Units

Much like the catch basins, regular maintenance of the water quality units is essential. The maintenance of these units begins immediately at post-construction prior to putting the unit into service. During the first year of operation, the units should be inspected quarterly in order to determine the rate of accumulation of sediment and oils. In subsequent years, the units can be inspected at a frequency determined by the accumulation rate of sediment and oils, but in no cases should the inspection frequency exceed six months.

Inspect and complete preventive maintenance in accordance with manufacturer's Recommendations (attached). Units should also be cleaned immediately in the event of a spill.

Existing 24" Culvert and Outlet Control Structures

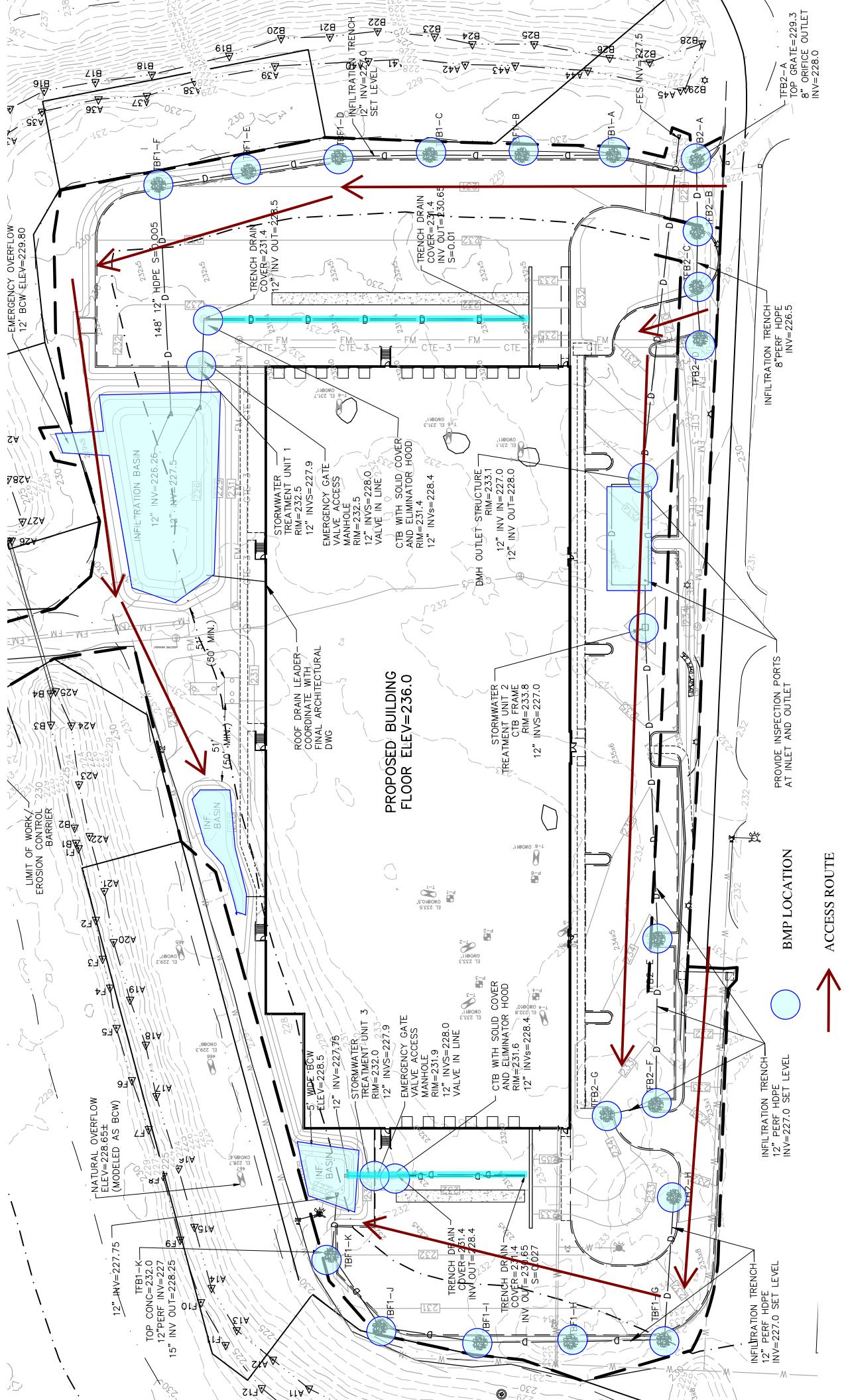
Inspect biannually. Inspect for structural soundness and confirm no blockage exists at openings, or within pipe; and no erosion is occurring at culvert or outlet control structure inlet or outlet. Remove trash, sediment, debris and vegetation. Restabilize area near inlets and outlets as necessary.

Infiltration Trenches

Inspect trenches every six months. Confirm inlet pipes are not blocked. Remove debris, as necessary.

Emergency Gate Valves

Emergency gate valves should be kept open. In case of a hazardous waste spill, close emergency gate valves to contain spill. Open and close emergency gate valves at least once yearly to confirm they are in good working condition.



Stormwater BMP Inspection and Maintenance Log

(print a log for each BMP and maintain a log book for the project)

BMP: _____

CDS® Inspection and Maintenance Guide



Maintenance

The CDS system should be inspected at regular intervals and maintained when necessary to ensure optimum performance. The rate at which the system collects pollutants will depend more heavily on site activities than the size of the unit. For example, unstable soils or heavy winter sanding will cause the grit chamber to fill more quickly but regular sweeping of paved surfaces will slow accumulation.

Inspection

Inspection is the key to effective maintenance and is easily performed. Pollutant transport and deposition may vary from year to year and regular inspections will help ensure that the system is cleaned out at the appropriate time. At a minimum, inspections should be performed twice per year (e.g. spring and fall) however more frequent inspections may be necessary in climates where winter sanding operations may lead to rapid accumulations, or in equipment washdown areas. Installations should also be inspected more frequently where excessive amounts of trash are expected.

The visual inspection should ascertain that the system components are in working order and that there are no blockages or obstructions in the inlet and separation screen. The inspection should also quantify the accumulation of hydrocarbons, trash, and sediment in the system. Measuring pollutant accumulation can be done with a calibrated dipstick, tape measure or other measuring instrument. If absorbent material is used for enhanced removal of hydrocarbons, the level of discoloration of the sorbent material should also be identified during inspection. It is useful and often required as part of an operating permit to keep a record of each inspection. A simple form for doing so is provided.

Access to the CDS unit is typically achieved through two manhole access covers. One opening allows for inspection and cleanout of the separation chamber (cylinder and screen) and isolated sump. The other allows for inspection and cleanout of sediment captured and retained outside the screen. For deep units, a single manhole access point would allow both sump cleanout and access outside the screen.

The CDS system should be cleaned when the level of sediment has reached 75% of capacity in the isolated sump or when an appreciable level of hydrocarbons and trash has accumulated. If absorbent material is used, it should be replaced when significant discoloration has occurred. Performance will not be impacted until 100% of the sump capacity is exceeded however it is recommended that the system be cleaned prior to that for easier removal of sediment. The level of sediment is easily determined by measuring from finished grade down to the top of the sediment pile. To avoid underestimating the level of sediment in the chamber, the measuring device must be lowered to the top of the sediment pile carefully. Particles at the top of the pile typically offer less resistance to the end of the rod than consolidated particles toward the bottom of the pile. Once this measurement is recorded, it should be compared to the as-built drawing for the unit to determine whether the height of the sediment pile off the bottom of the sump floor exceeds 75% of the total height of isolated sump.

Cleaning

Cleaning of a CDS system should be done during dry weather conditions when no flow is entering the system. The use of a vacuum truck is generally the most effective and convenient method of removing pollutants from the system. Simply remove the manhole covers and insert the vacuum hose into the sump. The system should be completely drained down and the sump fully evacuated of sediment. The area outside the screen should also be cleaned out if pollutant build-up exists in this area.

In installations where the risk of petroleum spills is small, liquid contaminants may not accumulate as quickly as sediment. However, the system should be cleaned out immediately in the event of an oil or gasoline spill should be cleaned out immediately. Motor oil and other hydrocarbons that accumulate on a more routine basis should be removed when an appreciable layer has been captured. To remove these pollutants, it may be preferable to use absorbent pads since they are usually less expensive to dispose than the oil/water emulsion that may be created by vacuuming the oily layer. Trash and debris can be netted out to separate it from the other pollutants. The screen should be power washed to ensure it is free of trash and debris.

Manhole covers should be securely seated following cleaning activities to prevent leakage of runoff into the system from above and also to ensure that proper safety precautions have been followed. Confined space entry procedures need to be followed if physical access is required. Disposal of all material removed from the CDS system should be done in accordance with local regulations. In many jurisdictions, disposal of the sediments may be handled in the same manner as the disposal of sediments removed from catch basins or deep sump manholes.



CDS Model	Diameter		Distance from Water Surface to Top of Sediment Pile		Sediment Storage Capacity	
	ft	m	ft	m	y ³	m ³
CDS1515	3	0.9	3.0	0.9	0.5	0.4
CDS2015	4	1.2	3.0	0.9	0.9	0.7
CDS2015	5	1.3	3.0	0.9	1.3	1.0
CDS2020	5	1.3	3.5	1.1	1.3	1.0
CDS2025	5	1.3	4.0	1.2	1.3	1.0
CDS3020	6	1.8	4.0	1.2	2.1	1.6
CDS3025	6	1.8	4.0	1.2	2.1	1.6
CDS3030	6	1.8	4.6	1.4	2.1	1.6
CDS3035	6	1.8	5.0	1.5	2.1	1.6
CDS4030	8	2.4	4.6	1.4	5.6	4.3
CDS4040	8	2.4	5.7	1.7	5.6	4.3
CDS4045	8	2.4	6.2	1.9	5.6	4.3
CDS5640	10	3.0	6.3	1.9	8.7	6.7
CDS5653	10	3.0	7.7	2.3	8.7	6.7
CDS5668	10	3.0	9.3	2.8	8.7	6.7
CDS5678	10	3.0	10.3	3.1	8.7	6.7

Table 1: CDS Maintenance Indicators and Sediment Storage Capacities



Support

- Drawings and specifications are available at www.contechstormwater.com.
- Site-specific design support is available from our engineers.

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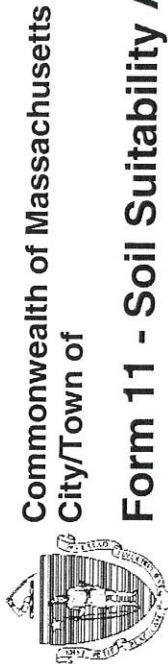
CDS Inspection & Maintenance Log

CDS Model: _____ Location: _____

Date	Water depth to sediment ¹	Floatable Layer Thickness ²	Describe Maintenance Performed	Maintenance Personnel	Comments

1. The water depth to sediment is determined by taking two measurements with a stadia rod: one measurement from the manhole opening to the top of the sediment pile and the other from the manhole opening to the water surface. If the difference between these measurements is less than the values listed in table 1 the system should be cleaned out. Note: to avoid underestimating the volume of sediment in the chamber, the measuring device must be carefully lowered to the top of the sediment pile.
2. For optimum performance, the system should be cleaned out when the floating hydrocarbon layer accumulates to an appreciable thickness. In the event of an oil spill, the system should be cleaned immediately.

Soils Data



Commonwealth of Massachusetts

City/Town of

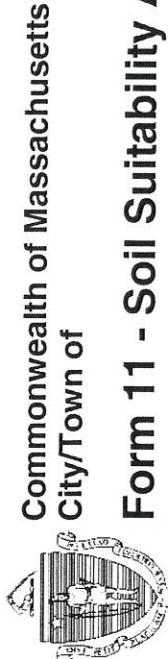
Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

A. Facility Information

Owner Name CDK-m&L, LLC
Street Address MONUMENT DRIVE
City LITTLETON State MA Zip Code 01460
Map/Lot # 210 16 B
Map Unit # 01460

B. Site Information

1. (Check one) New Construction Upgrade
2. Soil Survey NRCS Source 253D Soil Map Unit RAPID INFILTRATION
Landform STORY AND GRAYLEY Soil Limitations GENOFLUENT DEPOSITS Derived From GRANITE, SCHIST
Soil Parent material 2022 / Mass Mepper Year Published/Source Glaeble Stratified Deposits Map Unit GRANITE STRATIFIED DEPOSITS
3. Surficial Geological Report Glaeble Stratified Deposits Description of Geologic Map Unit: in layers Map Unit GRANITE STRATIFIED DEPOSITS
4. Flood Rate Insurance Map Within a regulatory floodway? Yes No
5. Within a velocity zone? Yes No
If yes, MassGIS Wetland Data Layer:
6. Within a Mapped Wetland Area? Yes No
7. Current Water Resource Conditions (USGS): 3/4/22 Month/Day/Year
Wetland Type Normal Below Normal
8. Other references reviewed:
(Zone II, IWPA, Zone A, EEA Data Portal, etc.) Mass GIS ; Littleton GIS



Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

C. On-Site Review (minimum of two holes required at every proposed primary and reserve disposal area)

Deep Observation Hole Number: D1+1 Date 3/4/22 Time 8:00 am Weather 40° Pthly cldy Latitude 42°31'01" Longitude 71°30'57"

1. Land Use Woodland
(e.g., woodland, agricultural field, vacant lot, etc.)

Description of Location: wooded undeveloped area

2. Soil Parent Material: Glaiofluvial Deposits Outwash Plain Landform

3. Distances from: Open Water Body 7750 feet Drainage Way 150± feet Wetlands 90± feet

Property Line 150± feet Drinking Water Well 720± feet Other _____ feet

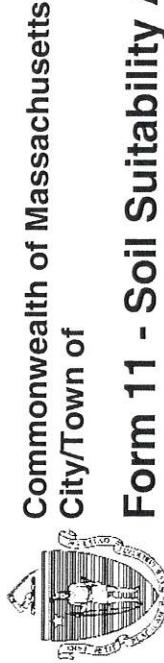
4. Unsuitable Materials Present: Yes No If Yes: Disturbed Soil/Fill Material Weathered/Fractured Rock Bedrock

5. Groundwater Observed: Yes No If yes: N/A Depth to Weeping in Hole 84" Depth to Standing Water in Hole

Soil Log

Depth (in)	Soil Horizon /Layer	Soil Texture (USDA)	Soil Matrix: Color-Moist (Munsell)	Redoximorphic Features			Coarse Fragments % by Volume		Soil Structure	Soil Consistency (Moist)	Other
				Depth	Color	Percent	Gravel	Cobbles & Stones			
0-4	A _p	F _{SL}	10YR 3/2	Cnc : Dpl:						FRIABLE	
4-20	B _s	F _{SL}	10YR 4/6	Cnc : Dpl:						FRIABLE	
20-120	C	F _{INE} S _{AND}	2.5Y 4/2 60"	Cnc : Dpl:						SANDY LOOSE	
				Cnc : Dpl:							
				Cnc : Dpl:							
				Cnc : Dpl:							
				Cnc : Dpl:							
				Cnc : Dpl:							

Additional Notes: _____



Commonwealth of Massachusetts
City/Town of

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

C. On-Site Review (minimum of two holes required at every proposed primary and reserve disposal area)

Deep Observation Hole Number:	Hole #	3/4/22	Date	8:15am	Time	45° Pky Cl dy	Weather	4231'01"	Latitude	71° 30' 57"	Longitude
1. Land Use:	(e.g. woodland, agricultural field, vacant lot, etc.)										
Description of Location:	wooded undeveloped area										
2. Soil Parent Material:	Glaciocluvial Deposits										
3. Distances from:	Open Water Body	750	feet	Landform	Outwash Plain					TS	
	Property Line	200	feet	Drainage Way	150	feet	Position on Landscape (SU, SH, BS, FS, TS, Plain)	Wetlands	135	feet	
	Drinking Water Well	720	feet	Other							
4. Unsuitable Materials Present:	<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No		If Yes:	<input type="checkbox"/> Disturbed Soil/Fill Material		<input type="checkbox"/> Weathered/Fractured Rock		<input type="checkbox"/> Bedrock			
5. Groundwater Observed:	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No		If yes:	105"		Depth to Weeping in Hole	84"			Depth Standing Water in Hole	

Soil Log

Depth (in)	Soil Horizon /Layer	Soil Texture (USDA)	Soil Matrix: Color-Moist (Munsell)	Redoximorphic Features			Coarse Fragments % by Volume	Soil Structure	Soil Consistency (Moist)	Other
				Depth	Color	Percent				
0-8	A _p	F _{SL}	10YR 3/2	Cnc : Dpl:						F2,1B,1E
8-24	B _u	F _{SL}	10YR 5/6	Cnc : Dpl:						F2,1B,1E
26-96	C	SAND	2.5Y 5/2 43'	Cnc : Dpl:			2%			SILTY LOAM
				Cnc : Dpl:						
				Cnc : Dpl:						
				Cnc : Dpl:						
				Cnc : Dpl:						
				Cnc : Dpl:						

Additional Notes:



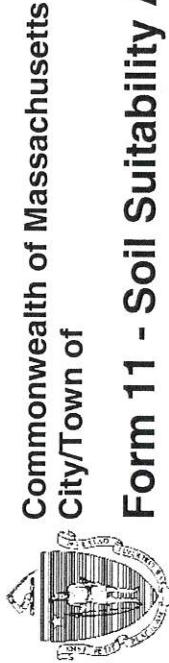
Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

C. On-Site Review (minimum of two holes required at every proposed primary and reserve disposal area)

Deep Observation Hole Number:	DT-3	Date	3/4/22	Time	8:30	Weather	42° 31' 01"	Latitude	71° 30' 57"
1. Land Use (e.g., woodland, agricultural field, vacant lot, etc.)	Woodland	Vegetation	Trees, scrub brush	Surface Stones (e.g., cobbles, stones, boulders, etc.)	Few large Boulders				
Description of Location:	Washed undeveloped area								
2. Soil Parent Material:	Glaciocluvial Deposits		Detached Plain		TS				
3. Distances from:	Open Water Body	780'	Landform	Drainage Way	190±	Position on Landscape (SU, SH, BS, FS, Plain)	Wetlands 120± feet		
	Property Line	240±	Drinking Water Well	200	feet	Other	feet		
4. Unsuitable Materials Present:	<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No		If Yes:	<input type="checkbox"/> Disturbed Soil/Fill Material		<input type="checkbox"/> Weathered/Fractured Rock		<input type="checkbox"/> Bedrock	
5. Groundwater Observed:	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No		If yes:	96"		Depth to Weeping in Hole			
Soil Log									

Depth (in)	Soil Horizon /Layer	Soil Texture (USDA)	Soil Matrix: Color-Moist (Munsell)	Redoximorphic Features			Coarse Fragments % by Volume		Soil Structure	Soil Consistency (Moist)	Other
				Depth	Color	Percent	Gravel	Cobbles & Stones			
0-22	A _p	FSL	10YR 3/2	Cnc : Dpl:							
22-35	B _w	FSL	10YR 5/6	Cnc : Dpl:							
35-99	C	SAND	2.5Y 6/2 62	Cnc : Dpl:							
				Cnc : Dpl:							
				Cnc : Dpl:							
				Cnc : Dpl:							
				Cnc : Dpl:							

Additional Notes:



Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

C. On-Site Review (minimum of two holes required at every proposed primary and reserve disposal area)

Deep Observation Hole Number: DT-4 Date 3/4/22 Time 9:00 am Weather 40° F Latitude 40° 31' 0" Longitude 71° 30' 57"
 1. Land Use: Woodland (e.g., woodland, agricultural field, vacant lot, etc.)
 Description of Location: wooded undeveloped land

2. Soil Parent Material: Glaciofluvial Deposits outwash plain Landform T5 Position on Landscape (SU, SH, BS, FS, TS, Plain)
 3. Distances from: Open Water Body 750 feet Drainage Way 240 feet Wetlands 140 feet
 Property Line 220 feet Drinking Water Well 220 feet Other feet

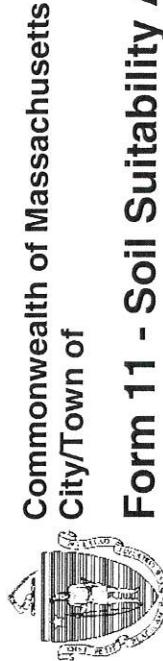
4. Unsuitable Materials Present: Yes No If Yes: Disturbed Soil/Fill Material Weathered/Fractured Rock Bedrock

5. Groundwater Observed: Yes No If yes: 71" Depth to Weeping in Hole 71" Depth Standing Water in Hole

Soil Log

Depth (in)	Soil Horizon /Layer	Soil Texture (USDA)	Soil Matrix: Color-Moist (Munsell)	Redoximorphic Features			Coarse Fragments % by Volume	Soil Structure	Soil Consistency (Moist)	Other
				Depth	Color	Percent				
0 - 3	O	FL	10YR 4/2	Cnc : Dpi:						
3 - 10	C	SAND	2.5Y 5/2 52"	Cnc : Dpi:			2 1/2	Sand-granular - loamy		
				Cnc : Dpi:						
				Cnc : Dpi:						
				Cnc : Dpi:						
				Cnc : Dpi:						
				Cnc : Dpi:						
				Cnc : Dpi:						

Additional Notes:



Commonwealth of Massachusetts
City/Town of

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

C. On-Site Review (minimum of two holes required at every proposed primary and reserve disposal area)

Deep Observation Hole Number:	Dt-5	Date	3/4/22	Time	9:15	Weather	40°	Latitude	42°31' 01"	Longitude	71°30' 57"
1. Land Use (e.g., woodland, agricultural field, vacant lot, etc.)	Woodland	Vegetation	tree, scrub brush	Surface Stones (e.g., cobbles, stones, boulders, etc.)	Few Large <u>Boulders</u>						
Description of Location:	undeveloped wooded area										
2. Soil Parent Material:	Glacio fluvial Deposits		Outwash Plain	TS	Position on Landscape (SU, SH, BS, FS, TS, Plain)						
3. Distances from:	Open Water Body	7800	feet	Drainage Way	1650	feet	Wetlands	400	feet	Other	_____ feet
	Property Line	2150	feet	Drinking Water Well	7200	feet					
4. Unsuitable Materials Present:	<input type="checkbox"/> Yes	<input checked="" type="checkbox"/> No	If Yes:	<input type="checkbox"/> Disturbed Soil/Fill Material	<input type="checkbox"/> Weathered/Fractured Rock	<input type="checkbox"/> Bedrock					
5. Groundwater Observed:	<input checked="" type="checkbox"/> Yes	<input type="checkbox"/> No	If yes:	<input type="checkbox"/> Depth to Weeping in Hole	81	feet	Depth to Standing Water in Hole				

Soil Log

Depth (in)	Soil Horizon /Layer	Soil Texture (USDA)	Soil Matrix: Color-Moist (Munsell)	Redoximorphic Features			Coarse Fragments % by Volume		Soil Structure	Soil Consistency (Moist)	Other
				Depth	Color	Percent	Gravel	Cobbles & Stones			
0-4	Ap	FSL	10YR 3/2								
6-18	Bw	FSL	10YR 5/6								
18-30	C	SAND	2.5Y 6/2 42"								

Additional Notes:



Commonwealth of Massachusetts
City/Town of

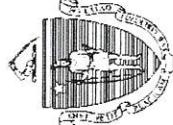
Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

C. On-Site Review (minimum of two holes required at every proposed primary and reserve disposal area)

Deep Observation Hole Number: <u>DT-6</u>	Date <u>3/4/22</u>	Time <u>9:30</u>	Latitude <u>42°31'01"</u>	Longitude <u>71°30'57"</u>
1. Land Use: <u>Woodland</u>	Vegetation <u>trees, scrub brush</u>	Weather <u>Few Large Precip.</u>	Surface Stones (e.g., cobbles, stones, boulders, etc.) <u>None</u>	
Description of Location: <u>wooded, undeveloped area</u>				
2. Soil Parent Material: <u>Glacio-fluvial Deposits</u>	Landform <u>Outwash Plain</u>	Position on Landscape (SU, SH, BS, FS, TS, Plain) <u>T3</u>		
3. Distances from:	Open Water Body <u>>200</u> feet	Drainage Way <u>145±</u> feet	Wetlands <u>15±</u> feet	Other <u>None</u> feet
	Property Line <u>175±</u> feet	Drinking Water Well <u>220</u> feet	<input type="checkbox"/> Weathered/Fractured Rock <input type="checkbox"/> Bedrock	
4. Unsuitable Materials Present: <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	If Yes: <input type="checkbox"/> Disturbed Soil/Fill Material	If Yes: <u>82"</u> Depth to Weeping in Hole <u>82"</u> Depth Standing Water in Hole		
5. Groundwater Observed: <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No				

Depth (in)	Soil Horizon /Layer	Soil Texture (USDA)	Soil Matrix: Color-Moist (Munsell)	Redoximorphic Features			Coarse Fragments % by Volume	Soil Structure	Soil Consistency (Moist)	Other
				Depth	Color	Percent				
0-2	A _p	FL	10YR 2/2	Cnc : Dpl:						
2-3	B _w	FL	10YR 5/2	Cnc : Dpl:						
3-6	C	SAND	2.5Y 6/2 8/1	Cnc : Dpl:						
6-12				Cnc : Dpl:						
				Cnc : Dpl:						
				Cnc : Dpl:						
				Cnc : Dpl:						
				Cnc : Dpl:						
				Cnc : Dpl:						
				Cnc : Dpl:						

Additional Notes:



Commonwealth of Massachusetts City/Town of

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

C. On-Site Review (minimum of two holes required at every proposed primary and reserve disposal area)

Deep Observation Hole Number: DHT-7	
Hole #	3/4/22
Date	9:45
Time	40° 7' 4" N
Weather	Cloudy
Latitude	42° 31' 0"
Longitude	71° 30' 57" W
1. Land Use (e.g., woodland, agricultural field, vacant lot, etc.)	Woodland
Description of Location:	wooded undeveloped area
2. Soil Parent Material:	Gleic fluvial Deposits
Landform	Outwash Plain
Position on Landscape (SU, SH, BS, ES, TS, Plain)	TS

3. Distances from: Open Water Body 130± feet Drainage Way 130± feet Wetlands 90 feet

Property Line 200± feet Drinking Water Well 200 feet Other _____ feet

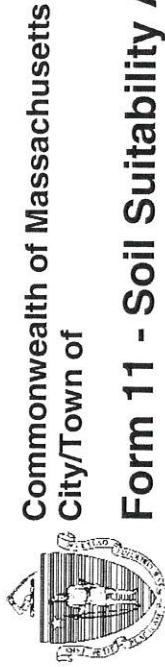
4. Unsuitable Materials Present: Yes No If Yes: Disturbed Soil/Fill Material Weathered/Fractured Rock Bedrock

5. Groundwater Observed: Yes No If Yes: 96" Depth to Weeping in Hole 76" Depth to Standing Water in Hole

Soil 13, 1000

Depth (in)	Soil Horizon /Layer	Soil Texture (USDA)	Soil Matrix: Color Moist (Munsell)	Redoximorphic Features			Coarse Fragments % by Volume			Soil Structure	Soil Consistence (Moist)	Other
				Depth	Color	Percent	Gravel	Cobbles & Stones				
0-3	O	10YR 2/2		Cnc : Dpl:								
3-98	C	2.5Y 4/2	10 ⁴	Cnc : Dpl:								

Additional Notes:



Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

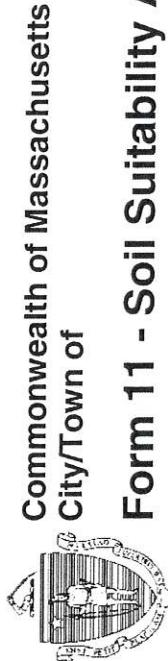
C. On-Site Review (minimum of two holes required at every proposed primary and reserve disposal area)

Deep Observation Hole Number:	DT-8	Date	3/4/22	Time	10:15	Weather	45° Phy/Chy	Latitude	42°31'01"	Longitude	71°30'57"
1. Land Use:	Woodland	(e.g., woodland, agricultural field, vacant lot, etc.)	Vegetation								
Description of Location:	wooded undeveloped area										
2. Soil Parent Material:	Glaciofluvial Deposits										
3. Distances from:	Open Water Body	1350± feet	Landform	Outwash Plan		Position on Landscape (SU, SH, BS, FS, TS, Plain)	Wetlands	103± feet			
Property Line	205± feet	Drainage Way	120± feet	Other	feet						
4. Unsuitable Materials Present:	<input type="checkbox"/> Yes	<input checked="" type="checkbox"/> No	If Yes:	<input type="checkbox"/> Disturbed Soil/Fill Material	<input type="checkbox"/> Weathered/Fractured Rock	<input type="checkbox"/> Bedrock					
5. Groundwater Observed:	<input checked="" type="checkbox"/> Yes	<input type="checkbox"/> No	If yes:	52"	Depth to Weeping in Hole	68"	Depth Standing Water in Hole				

Soil Log

Depth (in)	Soil Horizon /Layer	Soil Texture (USDA)	Soil Matrix: Color-Moist (Munsell)	Redoximorphic Features			Coarse Fragments % by Volume	Cobbles & Stones	Soil Structure	Soil Consistency (Moist)	Other
				Depth	Color	Percent					
0-4	D		10YR 2/2	Cnc:							
4-90	C	FINE SAND	2.5Y 4/1 28"	Dpl:							
				Cnc:							
				Dpl:							
				Cnc:							
				Dpl:							
				Cnc:							
				Dpl:							
				Cnc:							
				Dpl:							
				Cnc:							
				Dpl:							

Additional Notes:



Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

D. Determination of High Groundwater Elevation

1. Method Used (Choose one):

Depth to soil redoximorphic features

Depth to observed standing water in observation hole _____ inches

Depth to adjusted seasonal high groundwater (S_h)
(USGS methodology) _____ inches

Obs. Hole # DH-5

Obs. Hole # DH-4

Obs. Hole # DH-7

Obs. Hole # DH-8

42" inches

84" inches

10" inches

28" inches

Index Well Number _____ Reading Date _____

$$S_h = S_c - [S_r \times (OW_c - OW_{max})/OW_r]$$

Obs. Hole/Well# _____ S_c _____ S_r _____

OW_c _____ OW_r _____ OW_{max} _____

OW_h _____

E. Certification

I certify that I am currently approved by the Department of Environmental Protection pursuant to 310 CMR 15.017 to conduct soil evaluations and that the above analysis has been performed by me consistent with the required training, expertise and experience described in 310 CMR 15.017. I further certify that the results of my soil evaluation, as indicated in the attached Soil Evaluation Form, are accurate and in accordance with 310 CMR 15.100 through 15.107.

Jeffrey S. Gareff

Signature of Soil Evaluator

Typed or Printed Name of Soil Evaluator/License #

Patrick J. Burke II / SE278

Date 4/8/22

Expiration Date of License

6/30/22

Approving Authority

N Abbott

Name of Approving Authority Witness

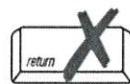
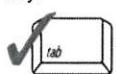
James Gareff



Commonwealth of Massachusetts
City/Town of
Percolation Test
Form 12

Percolation test results must be submitted with the Soil Suitability Assessment for On-site Sewage Disposal. DEP has provided this form for use by local Boards of Health. Other forms may be used, but the information must be substantially the same as that provided here. Before using this form, check with the local Board of Health to determine the form they use.

Important: When filling out forms on the computer, use only the tab key to move your cursor - do not use the return key.



CDK-MEC, LLC

Owner Name

MONARCH DRIVE

Street Address or Lot #

LITTLETON

City/Town

MA

01460

Zip Code

Contact Person (if different from Owner)

Telephone Number

A. Site Information

B. Test Results

Observation Hole #

3/4/22

12:56

PT-1

3/4/22

11:29

PT-2

Depth of Perc

33" shelf

34" shelf

Start Pre-Soak

12:56 pm

1:21 pm

End Pre-Soak

1:14 pm

1:36 pm

Time at 12"

1:14 pm

1:36 pm

Time at 9"

1:15 pm

1:42 pm

Time at 6"

1:17 pm

1:47 pm

Time (9"-6")

2 min

5 min

Rate (Min./Inch)

<2 min/inch

<2 min/inch

Test Passed:



Test Passed:



Test Failed:

Test Performed By:

Patrick J. Burke SIE 278

Board of Health Witness

Comments:

PT-1 tested next to DH-1

PT-2 tested next to DH-3



Commonwealth of Massachusetts

City/Town of

Percolation Test

Form 12

Percolation test results must be submitted with the Soil Suitability Assessment for On-site Sewage Disposal. DEP has provided this form for use by local Boards of Health. Other forms may be used, but the information must be substantially the same as that provided here. Before using this form, check with the local Board of Health to determine the form they use.

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A. Site Information

CDK-MCL, LLC

Owner Name

MONARCH DRIVE

Street Address or Lot #

LITTLETON

City/Town

MA

01460

State

Zip Code

Contact Person (if different from Owner)

Telephone Number

B. Test Results

Observation Hole #

3/4/22

Time

PT-3

Depth of Perc

24" Shelf

3/4/22

Time

PT-4

Start Pre-Soak

12:29 pm

30" Shelf

End Pre-Soak

12:44 pm

12:42

Time at 12"

12:44 pm

12:57

Time at 9"

1:30 pm

24 gallons

Time at 6"

2:19 pm

poured

Time (9"-6")

49 MIN

Rate (Min./Inch)

17 MIN/INCH

Test Passed:



Test Passed:



Test Failed:

Patrick J. Burke S# 288

Test Performed By:

James Garreffa

Board of Health Witness

Comments:

PT-3 tested next to DH-7

PT-4 tested next to DH-6



PLACES

Associates, Inc.

Planning
Landscape Architecture
Civil Engineering
Surveying

SOILS OBSERVATION AND TESTING REPORT

Site Location: Monarch Drive, Littleton, MA
Project No.: 5554
Date: 03/04/2022
Time of Testing: 2:00 PM

Weather No precipitation
Temp: 45° F
Sky Condition: Partly Cloudy

Notes:

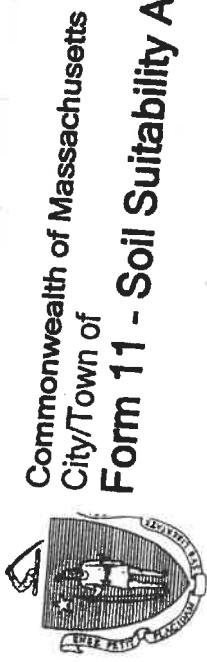
SW #1: 0"-1" Organic
1"-96" Sand, single grain loose
No groundwater observed
No Redox observed

SW #2: 0"-2" Organic
1"-78" Sand, single grain loose
No groundwater observed
Redox @72"

SW #3: 0"-2" Organic
1"-96" Sand, single grain loose
No groundwater observed
Redox @58"

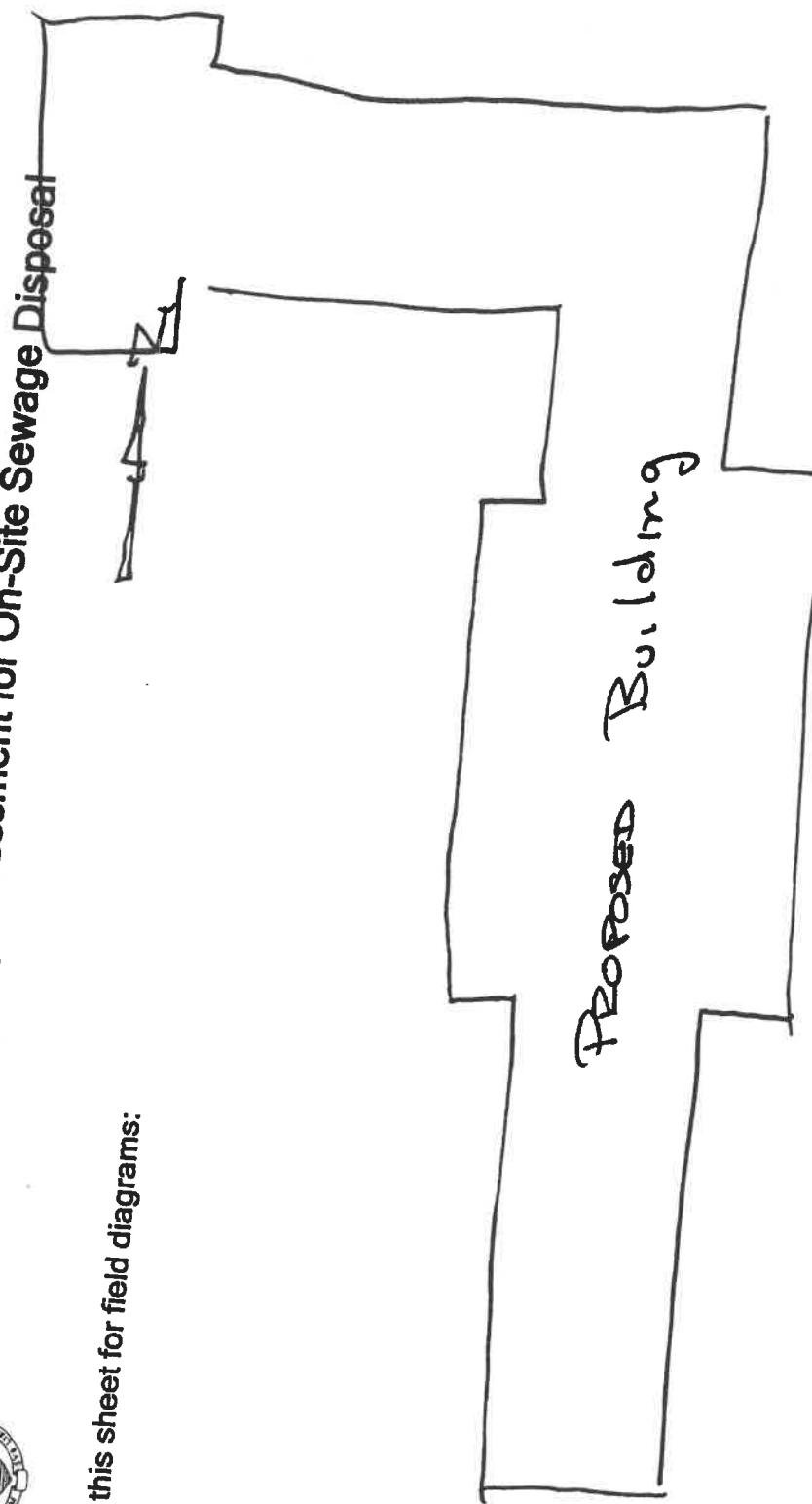
SW #4: 0"-3" Organic
3"-140" Sand, single grain loose
Groundwater observed weeping@140"
No Redox observed

Plot



Commonwealth of Massachusetts
City/Town of
Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

Use this sheet for field diagrams:



465 460 867



Commonwealth of Massachusetts
City/Town of Litchfield
Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

D. Determination of High Groundwater Elevation

1. Method used:

- Depth observed standing water in observation hole A. 126 inches
- Depth weeping from side of observation hole A. 126 inches
- Depth to soil redoximorphic features (mottles) A. 124 inches
- Groundwater adjustment (USGS methodology) A. _____ inches

E. Depth of Pervious Material

1. Depth of Naturally Occurring Pervious Material

- a. Does at least four feet of naturally occurring pervious material exist in all areas observed throughout the area proposed for the soil absorption system? Yes No
- b. If yes, at what depth was it observed? Upper boundary: _____ inches Lower boundary: _____ inches

F. Certification

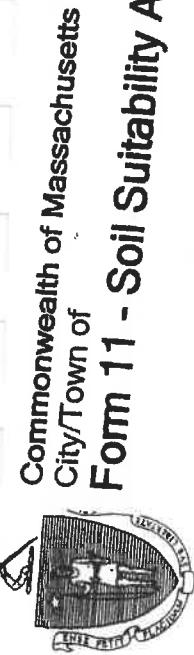
I certify that I am currently approved by the Department of Environmental Protection pursuant to 310 CMR 15.017 to conduct soil evaluations and that the above analysis has been performed by me consistent with the required training, expertise and experience described in 310 CMR 15.017. I further certify that the results of my soil evaluation, as indicated in the attached Soil Evaluation Form, are accurate and in accordance with 310 CMR 15.100 through 15.107.

Gordon R. Johnson
Signature of Soil Evaluator
Gordon R. Johnson
Typed or Printed Name of Soil Evaluator/License Number
Date 2014

Nov. 1994
Date
*Date of Soil Evaluator Exam

Jim Gitterelli
Name of Board of Health Witness
Jim Gitterelli
Dave Boyce (PES)
Date 11/17/2012
Board of Health

Note: In accordance with 310 CMR 15.018(2) this form must be submitted to the approving authority within 60 days of the date of field testing, and to the designer and the property owner with Percolation Test Form 12.



Commonwealth of Massachusetts
City/Town of _____

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

C. On-Site Review (Cont.)

Deep Observation Hole Number: T-1

Date 4-8-08

Ground Elevation at Surface of Hole _____

Location (Identify on Plan) _____

Sunny 50°
Weather

Time _____

Slope (%) _____

Land Use: FIELD

(e.g. woodland, agricultural field, vacant lot, etc.)

Vegetation Grasses

Landform _____

Surface Stones _____

Position on landscape (attach sheet) A

Slope (%) _____

Distances from: Open Water Body feet _____

Drainage Way feet _____

Possible Wet Area feet _____

Drinking Water Well feet _____

Other feet _____

feet _____

Parent Material: Glacial Outwash

Unsuitable Materials Present: Yes No

Disturbed Soil

Fill Material

Impervious Layer(s)

Weathered/Fractured Rock

Bedrock

Weathered Rock

Fractured Rock

Bedrock

No

Yes

No

Yes

No

No

Yes

No

Yes

No

If Yes: Depth Weeping from Pit 126

Depth Standing Water in Hole 126

Estimated Depth to High Groundwater: 126

inches _____

elevation _____



Commonwealth of Massachusetts
City/Town of Leominster
Form 11 - Soil Suitability A

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

Deep Observation Hole Number: 7-1

Depth (in.)	Soil Horizon/ Layer	Soil Matrix: Color-Moist (Munsell)	Redoximorphic Features (mottles)	Soil Texture (USDA)			Coarse Fragments % by Volume		Soil Structure	Soil Consistence (Moist)	Other
				Depth	Color	Percent	Gravel	Cobbles & Stones			
0 - 12 -	Bw	10 YR 5/6					1/5	0	0%	m	muf
12 - 132	C	2.5 Y 6/3	126				CS	30	0%	39	muf

Additional Notes



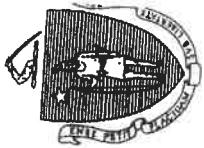
**Commonwealth of Massachusetts
City/Town of _____
Form 11 - Soil Suitability /**

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

Deep Observation Hole Number: 7-2

Depth (In.)	Soil Horizon/ Layer	Soil Matrix: Color-Moist (Munsell)	Redoximorphic Features (mottles)		Soil Texture (USDA)	Coarse Fragments % by Volume	Soil Structure	Soil Consistence (Moist)	Other
			Depth	Color					
0 - 10	Bw	10YR 5/6			1S	0	m	muf	
10 - 96	C ₁	2.5Y 6/4			m/c 5	0	%	ss	muf
96 - 144	C ₂	2.5Y 9/3	132		CS	30	%	ss	muf

Additional Notes

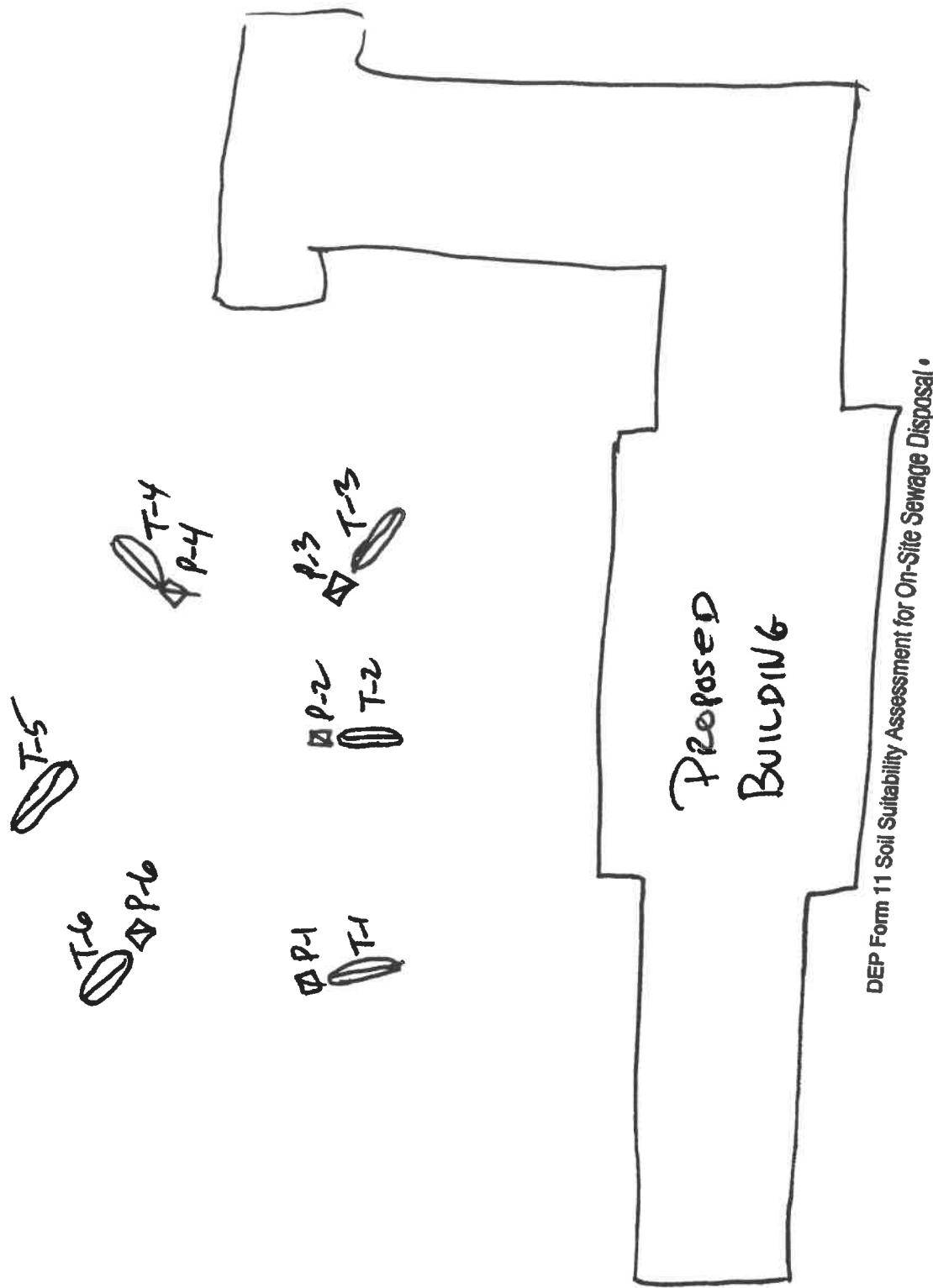


Commonwealth of Massachusetts
City/Town of

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

B/T. Drive

Use this sheet for field diagrams:





Commonwealth of Massachusetts
City/Town of LITTLETON
Percolation Test
Form 12

HAYES ENGR., INC.
603 SALEM STREET
WAKEFIELD, MA 01880
TELEPHONE (617) 246-2800
FAX (617) 246-7596

Important:
When filling out
forms on the
computer, use
only the tab key
to move your
cursor - do not
use the return
key.



Percolation test results must be submitted with the Soil Suitability Assessment for On-site Sewage Disposal. DEP has provided this form for use by local Boards of Health. Other forms may be used, but the information must be substantially the same as that provided here. Before using this form, check with the local Board of Health to determine the form they use.

A. Site Information

Owner Name Waterford Development
Street Address or Lot # 175 HIGHLAND AVE
City/Town NEEDHAM State MA Zip Code _____
Contact Person (if different from Owner) _____ Telephone Number _____

B. Test Results

Observation Hole #

4-8-08
Date _____ Time _____
P-1

Depth of Perc

18" + 18" = 36"
Date _____ Time _____

Start Pre-Soak

9:14

4-8-08
Date _____ Time _____
P-2

End Pre-Soak

21" + 18" = 39"
Date _____ Time _____

Time at 12"

9:16

9:18
Date _____ Time _____

Time at 9"

25 gals
Date _____ Time _____

Time at 6"

9:17

9:29
Date _____ Time _____

Time (9"-6")

< 2 ml

9:32
Date _____ Time _____

Rate (Min./Inch)

9:35
Date _____ Time _____

3
Date _____ Time _____

< 2 ml

Test Passed:
Test Failed:

Test Passed:
Test Failed:

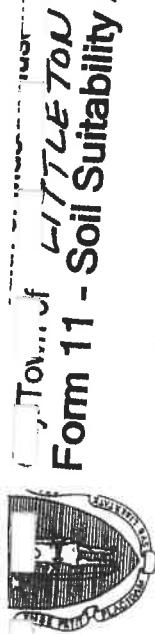
Gordon Rogerson

Test Performed By:

Dave Boyer (DEP)

Witnessed By:

Comments:



MONARCH DRIVE

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

JOB FILE

667-0007

DEP has provided this form for use by on-site professionals and local Boards of Health. Other forms may be used, but the information must be substantially the same as provided here. Before using this form, check with your local Board of Health to determine the form they use.

A. Facility Information

1. Facility Information

WATERFORD DEVELOPMENT

175 HIGHLAND Ave

Map/Lot

NEEDHAM

MA

State

02495

Zip Code

HAYES ENGINEERING, INC.
603 SALEM STREET
WAKEFIELD, MA 01880
TEL: 781-226-2800
FAX: 781-226-7596

B. Site Information

1. (Check one) New Construction Upgrade Repair
2. Published Soil Survey available? Yes No If yes: _____

Soil Name

3. Surficial Geological Report available? Yes No If yes: _____

Geologic Material

4. Flood Rate Insurance Map:

Above the 500 year flood boundary? Yes No
Within the 500 year flood boundary? Yes No

5. Wetland Area: National Wetland Inventory Map

Wetlands Conservancy Program Map

Map Unit

Map Unit

Name

Name

Range

Range

Above Normal

Above Normal

Normal

Normal

Below Normal

Below Normal

7. Other references reviewed: _____

Commonwealth of Massachusetts
City/Town of _____
Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal



D. Determination of High Groundwater Elevation

1. Method used:

- Depth observed standing water in observation hole A. 132 inches B. 120 inches
- Depth weeping from side of observation hole A. 132 inches B. 120 inches
- Depth to soil redoximorphic features (mottles) A. 132 inches B. 120 inches
- Groundwater adjustment (USGS methodology) A. _____ inches B. _____ inches

2. Index Well Number _____ Reading Date _____ Index Well Level _____
Adjustment Factor _____ Adjusted Groundwater Level _____

E. Depth of Pervious Material

1. Depth of Naturally Occurring Pervious Material

a. Does at least four feet of naturally occurring pervious material exist in all areas observed throughout the area proposed for the soil absorption system? Yes No

b. If yes, at what depth was it observed? Upper boundary: _____ inches Lower boundary: _____ inches

F. Certification

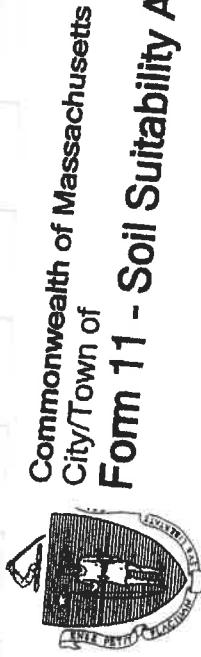
I certify that I am currently approved by the Department of Environmental Protection pursuant to 310 CMR 15.017 to conduct soil evaluations and that the above analysis has been performed by me consistent with the required training, expertise and experience described in 310 CMR 15.017. I further certify that the results of my soil evaluation, as indicated in the attached Soil Evaluation Form, are accurate and in accordance with 310 CMR 15.100 through 15.107.

Gordon J. Roger
Signature of Soil Evaluator
Gordon J. Roger, SE 2074
Typed or Printed Name of Soil Evaluator/License Number
Tim Greenfield Dave Boyce (Ded)
Name of Board of Health Witness

April 9, 2008
Date Apr. 9, 1994
Date of Soil Evaluator Exam

L. H. Peterson
Board of Health

Note: In accordance with 310 CMR 15.018(2) this form must be submitted to the approving authority within 60 days of the date of field testing, and to the designer and the property owner with Percolation Test Form 12.



Commonwealth of Massachusetts
City/Town of _____

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

C. On-Site Review (Cont.)

Deep Observation Hole Number: 7-3

4-8-08

Date

Time

Sunny 50°

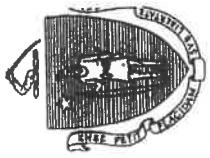
Weather

Ground Elevation at Surface of Hole _____

Location (Identify on Plan) _____

1. Location

2. Land Use: <u>Field</u> (e.g. woodland, agricultural field, vacant lot, etc.)	Vegetation: <u>Grasses</u>	Landform: <u>Wd</u>	Slope (%): <u>A</u>
3. Distances from: Open Water Body <u>feet</u>	Drainage Way <u>feet</u>	Possible Wet Area <u>feet</u>	Position on landscape (attach sheet)
Property Line <u>feet</u>	Drinking Water Well <u>feet</u>	Other <u>feet</u>	
4. Parent Material: <u>Glacial Outwash</u>	Unsuitable Materials Present: Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>		
If Yes: Disturbed Soil <input type="checkbox"/> Fill Material <input type="checkbox"/> Impervious Layer(s) <input type="checkbox"/> Weathered/Fractured Rock <input type="checkbox"/> Bedrock <input type="checkbox"/>			
5. Groundwater Observed: Yes <input checked="" type="checkbox"/> No <input type="checkbox"/>			
If Yes: Depth Weeping from Pit <u>13 2</u>	Depth Standing Water in Hole <u>13 2</u>	inches	elevation
Estimated Depth to High Groundwater: <u>13 2</u>			



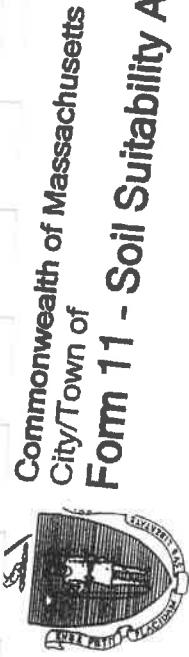
Commonwealth of Massachusetts
City/Town of _____
Form 11 - Soil Suitability /

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

T-3

Deep Observation Hole Number: _____

Additional Notes



Commonwealth of Massachusetts
City/Town of _____

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

C. On-Site Review (Cont.)

Deep Observation Hole Number: 7-4

1. Location

Ground Elevation at Surface of Hole _____
Location (Identify on Plan) _____

Date _____

Time _____

Sunny 50°
Weather

2. Land Use: Forest

(e.g. woodland, agricultural field, vacant lot, etc.)
Forests

Vegetation

3. Distances from: Open Water Body 0 feet
Property Line 0 feet
Drainage Way 0 feet
Drinking Water Well 0 feet
Possible Wet Area 0 feet
Other 0 feet

Position on landscape (attach sheet)

Landform A

Surface Stones N/A

Slope (%) 0

4. Parent Material: Glacial Drift/wash

If Yes: Disturbed Soil Fill Material

Impervious Layer(s)

Unsuitable Materials Present: Yes No

Weathered/Fractured Rock Bedrock

5. Groundwater Observed: Yes No

If Yes: Depth Weeping from Pit 120 inches

Estimated Depth to High Groundwater: 120 inches
Depth Standing Water in Hole 110 inches

elevation _____



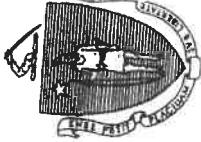
Commonwealth of Massachusetts
City/Town of *Lynnfield*
Form 11 - Soil Suitability /

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

Deen Observation Hole Number: T-4

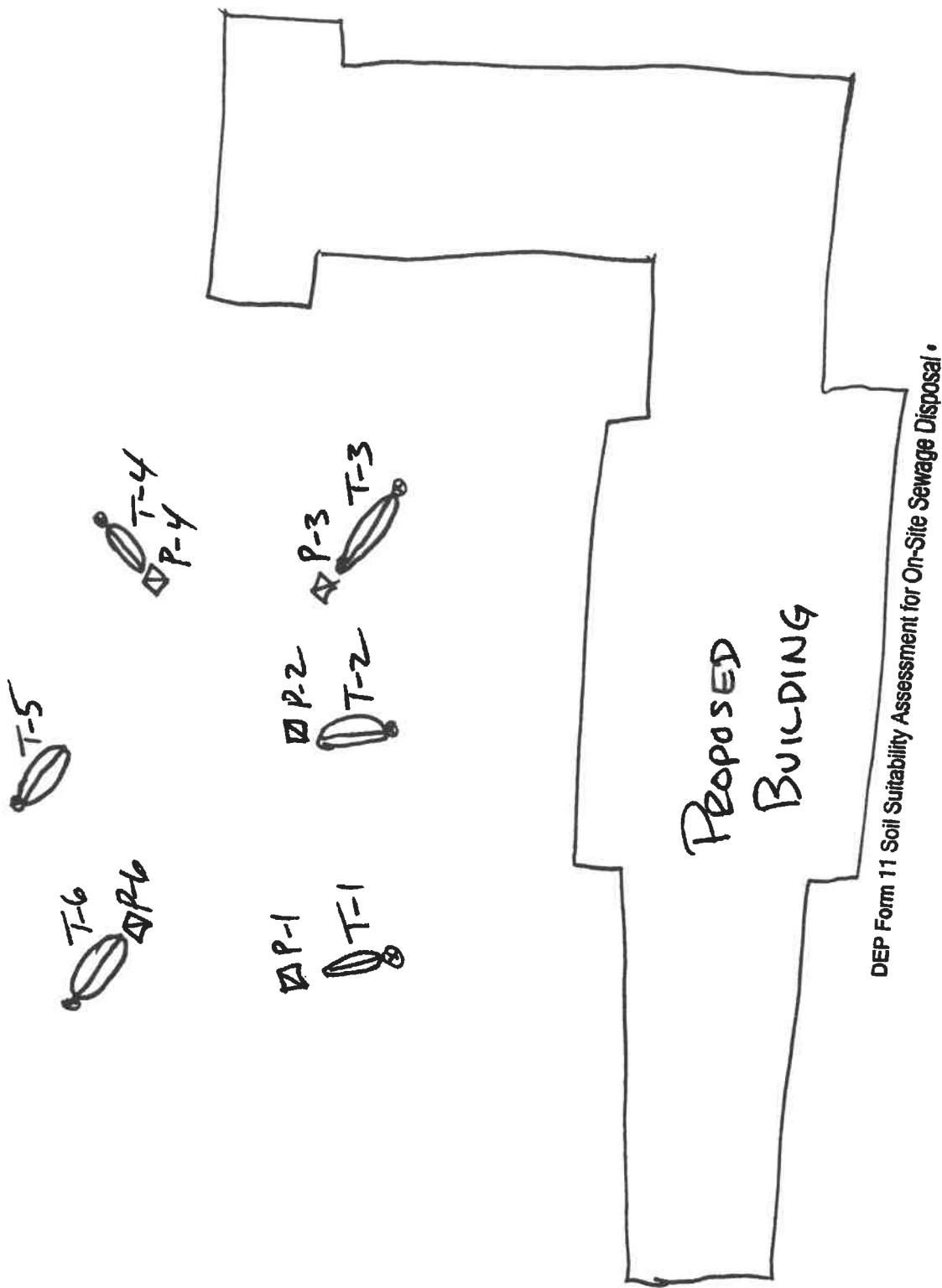
Depth (In.)	Soil Horizon/Layer	Soil Matrix: Color-Moist (Munsell)	Redoximorphic Features (mottles)		Soil Texture (USDA)	Coarse Fragments % by Volume	Soil Structure	Soil Consistency (Moist)	Other
			Depth	Color					
0 - 1.3	Bw	10YR 5/6			s	0	m	mf	
1.3 - 12.6	C	2.5Y 6/4	120		m/c	0	59	mf	
					s				

Additional Notes



Commonwealth of Massachusetts
City/Town of Uxbridge
Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

Use this sheet for field diagrams:





Commonwealth of Massachusetts
City/Town of **LITTLETON**
Percolation Test
Form 12

HAYES ENGR. INC.
603 SALEM STREET
WAKEFIELD, MA 01880
TEL (978) 246-2800
FAX (978) 246-7596

Important:
When filling out
forms on the
computer, use
only the tab key
to move your
cursor - do not
use the return
key.



Percolation test results must be submitted with the Soil Suitability Assessment for On-site Sewage Disposal. DEP has provided this form for use by local Boards of Health. Other forms may be used, but the information must be substantially the same as that provided here. Before using this form, check with the local Board of Health to determine the form they use.

A. Site Information

Waterford Development

Owner Name

179 HIGHLAND

Street Address or Lot #

City/Town

NEEDHAM

MA

Zip Code

Telephone Number

B. Test Results

Observation Hole #

4-8-08

Date P-3

Time

4-8-08

Date P-4

Time

Depth of Perc

30" 18" 48"

Time

28" 18" 46"

Start Pre-Soak

9:37

9:57

End Pre-Soak

25gals

25gals

Time at 12"

9:49

10:08

Time at 9"

9:51

10:09

Time at 6"

9:56

10:11

Time (9"-6")

5

2

Rate (Min./Inch)

<2m/l

<2m/l

Test Passed:



Test Passed:



Test Failed:

Gordon Rogerson

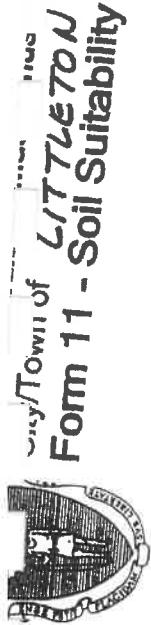
Test Performed By:

DAVE BOYER (DEP)

Witnessed By:

Comments:

MONARCH DRIVE



Monachus Drive

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

On-Site Sewage Disposal

DEP has provided this form for use by on-site professionals and local Boards of Health. Other forms may be used, but the information must be substantially the same as provided here. Before using this form, check with your local Board of Health to determine the form they use.

A. Facility Information

1. Facility Information

Owner Name WATERFORD DEVELOPMENT
Street Address 1754 HARRISON AVE
City/Town NEW BRUNSWICK Map/Lot 02494
State MA. Zip Code 01880-2800

HAYES ENGINEERING, INC.

603 SALEM STREET
WAKEFIELD, MA 01880
TEL: 781-226-7596
FAX: 781-226-7596

T-5 + T-6

B. Site Information

1. (Check one) New Construction Upgrade Repair
2. Published Soil Survey Available? Yes No If yes: _____

Soil Name _____

Year Published _____

Publication Scale _____

Soil Map Unit _____

Map Unit _____

3. Surficial Geological Report Available? Yes No If yes: _____

Geologic Material _____

Year Published _____

Publication Scale _____

Soil Map Unit _____

Map Unit _____

4. Flood Rate Insurance Map:

Above the 500 year flood boundary? Yes No
Within the 500 year flood boundary? Yes No

Within the 100 year flood boundary? Yes No

Within a Velocity Zone? Yes No

5. Wetland Area: National Wetland Inventory Map

Wetlands Conservancy Program Map

Map Unit _____

Map Unit _____

Name _____

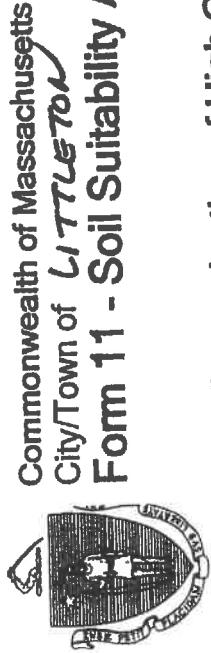
Name _____

6. Current Water Resource Conditions (USGS)

Range: Above Normal Normal

Below Normal

7. Other references reviewed:



Commonwealth of Massachusetts City/Town of UPTON Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

D. Determination of High Groundwater Elevation

1. Method used:

- Depth observed standing water in observation hole A. 132 inches
- Depth weeping from side of observation hole A. 132 inches
- Depth to soil redoximorphic features (mottles) A. 132 inches
- Groundwater adjustment (USGS methodology) A. 132 inches

2. Index Well Number _____ Reading Date _____ Index Well Level _____
Adjustment Factor _____ Adjusted Groundwater Level _____

E. Depth of Pervious Material

1. Depth of Naturally Occurring Pervious Material

a. Does at least four feet of naturally occurring pervious material exist in all areas observed throughout the area proposed for the soil absorption system? Yes No

b. If yes, at what depth was it observed? Upper boundary: _____ inches Lower boundary: _____ inches

F. Certification

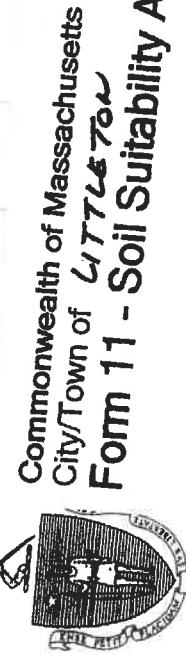
I certify that I am currently approved by the Department of Environmental Protection pursuant to 310 CMR 15.017 to conduct soil evaluations and that the above analysis has been performed by me consistent with the required training, expertise and experience described in 310 CMR 15.017. I further certify that the results of my soil evaluation, as indicated in the attached Soil Evaluation Form, are accurate and in accordance with 310 CMR 15.100 through 15.107.

Roger J. Gordon
Signature of Soil Evaluator
Gordon ROGER SON
Typed or Printed Name of Soil Evaluator/License Number
Name of Board of Health Witness

Nov. 1994
Date
C. THOMAS
Signature
Board of Health

SE 1074
Signature of Soil Evaluator
Gordon ROGER SON
Typed or Printed Name of Soil Evaluator/License Number
Name of Board of Health Witness

Note: In accordance with 310 CMR 15.018(2) this form must be submitted to the approving authority within 60 days of the date of field testing, and to the designer and the property owner with Percolation Test Form 12.



Commonwealth of Massachusetts
City/Town of *Wellesley*
Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

C. On-Site Review (Cont.)

Deep Observation Hole Number: T-5 4-8-08

1. Location

Ground Elevation at Surface of Hole _____

Location (Identify on Plan) _____

Date

Time

Sunny 50°
Weather

2. Land Use: Field

(e.g. woodland, agricultural field, vacant lot, etc.)

Grasses
Vegetation

3. Distances from: Open Water Body _____
Property Line _____
Drainage Way _____
Drinking Water Well _____
Surface Stones _____

Landform

Slope (%)

4. Parent Material: Glacial Outwash
If Yes: Disturbed Soil Fill Material Impervious Layer(s) Unsuitable Materials Present: Yes No

Possible Wet Area
feet _____
feet _____
feet _____
feet _____

Position on landscape (attach sheet)

5. Groundwater Observed: Yes No

If Yes: Depth Weeping from Pit 132 inches _____

Estimated Depth to High Groundwater: 132 inches _____

Depth Standing Water in Hole _____

Bedrock

elevation _____



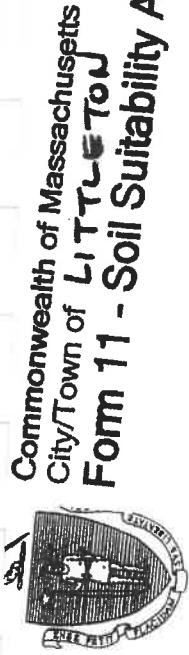
Commonwealth of Massachusetts
City/Town of LAWRENCE
Form 11 - Soil Suitability A

City/Town of *L77&78*
Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

Door Observation Hole Number: T-5

Depth (in.)	Soil Horizon/ Layer	Soil Matrix: Color-Moist (Munsell)	Redoximorphic Features (mottles)		Soil Texture (USDA)	Coarse Fragments % by Volume		Soil Structure	Soil Consistence (Moist)	Other
			Depth	Color		Gravel	Cobbles & Stones			
0-9	Bw	10YR 5/6			1/2	0	0%	m	muf	
9-14	C	2.5Y 3/4	132		m/c	0	0%	59	muf	

Additional Notes



C. On-Site Review (Cont.)

Deep Observation Hole Number:

7-6

4-8-08

Date

Time

Sunny 50°

Weather

Ground Elevation at Surface of Hole

Location (Identify on Plan)

1. Location

Vegetation
Grasses

2. Land Use: Field

(e.g. woodland, agricultural field, vacant lot, etc.)

No

Surface Stones

A

Slope (%)

Landform

Position on landscape (attach sheet)

3. Distances from: Open Water Body feet Drainage Way feet Possible Wet Area feet

Property Line feet

Drinking Water Well feet

Other feet

4. Parent Material: Glacial Outwash

If Yes: Disturbed Soil Fill Material Impermeous Layer(s) Weathered/Fractured Rock Bedrock

Unsuitable Materials Present: Yes No

5. Groundwater Observed: Yes No

If Yes: Depth Weeping from Pit 132

Estimated Depth to High Groundwater: 132

inches

elevation



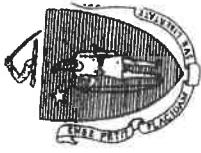
Commonwealth of Massachusetts
City/Town of *LAWRENCE*
Form 11 - Soil Suitability /

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

Deep Observation Hole Number. 7-6

Depth (in.)	Soil Horizon/ Layer	Soil Matrix: Color-Moist (Munsell)	Redoximorphic Features (mottles)		Soil Texture (USDA)	Coarse Fragments % by Volume		Soil Structure	Soil Consistency (Moist)	Other
			Depth	Color		Percent	Gravel			
0 - 6	Bw	10YR 5/6			15	0	0%	m	m/f	
6 - 15	C	2.5Y 6/4	132		m/c	30	0%	39	m/f	
					s					

Additional Notes -



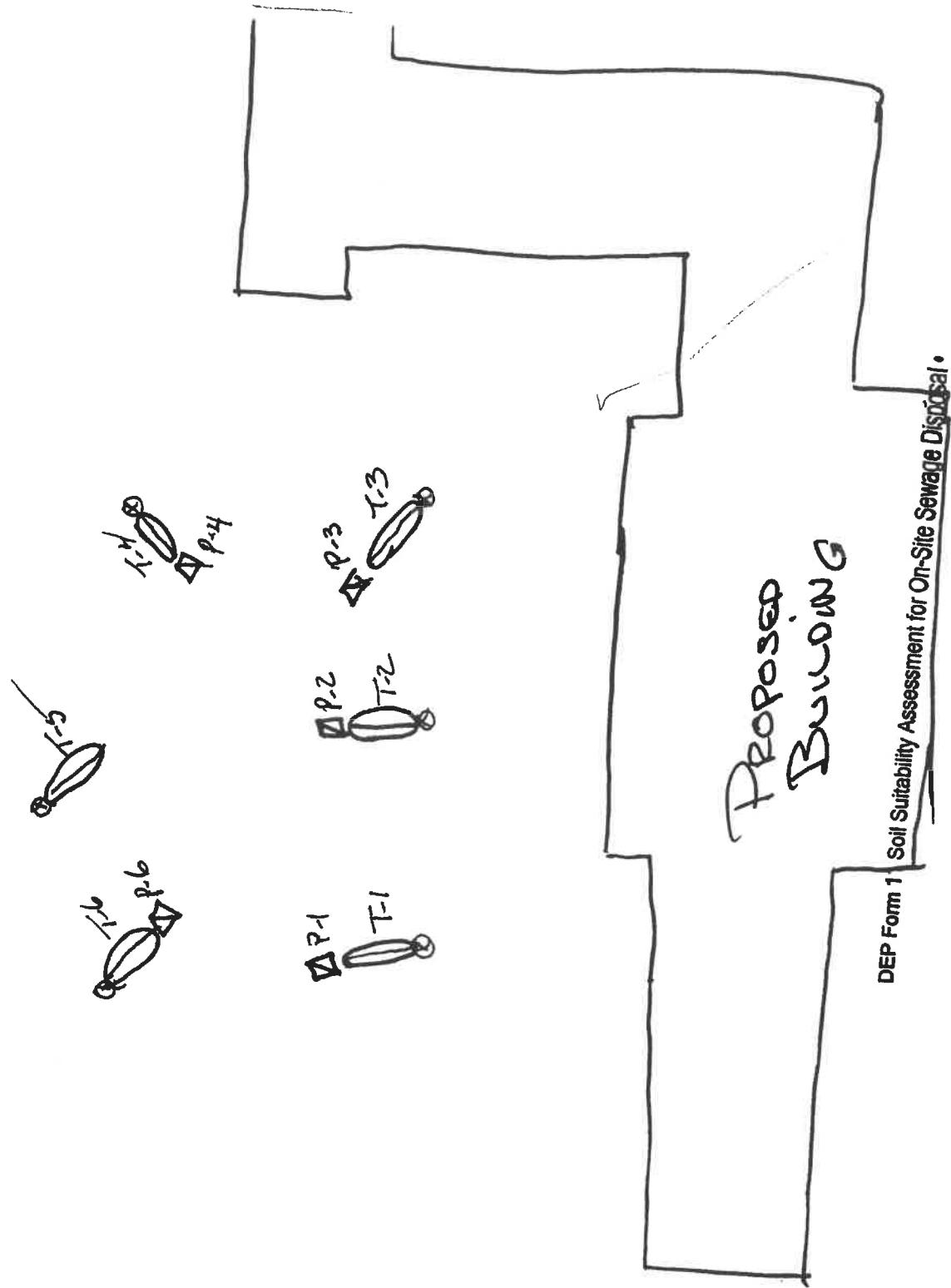
Commonwealth of Massachusetts

City/Town of LITTLETON

Br. T. Drive

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

Use this sheet for field diagrams:





Commonwealth of Massachusetts
City/Town of **LITTLETON**
Percolation Test
Form 12

HAYES ENGINEERING, INC.
603 SALEM STREET
WAKEFIELD, MA 01880
Tel: (978) 246-2800
Fax: (978) 246-7596

Important:
When filling out
forms on the
computer, use
only the tab key
to move your
cursor - do not
use the return
key.



Percolation test results must be submitted with the Soil Suitability Assessment for On-site Sewage Disposal. DEP has provided this form for use by local Boards of Health. Other forms may be used, but the information must be substantially the same as that provided here. Before using this form, check with the local Board of Health to determine the form they use.

A. Site Information

Owner Name **WATERFORD DEVELOPMENT**
Street Address or Lot # **179 HIGHLAND AVE**
City/Town **NEEDHAM** State **MA** Zip Code _____
Contact Person (if different from Owner) _____ Telephone Number _____

B. Test Results

Observation Hole #	Date	Time	4-8-08
Depth of Perc	Date	Time	P-6
Start Pre-Soak			22" + 18" = 40"
End Pre-Soak			10:06
Time at 12"			25gols
Time at 9"			10:08
Time at 6"			10:09
Time (9"-6")			10:10
Rate (Min./Inch)			1
			<2m/l

Gordon Rogerson
Test Performed By:

Test Passed:
Test Failed:

Test Passed:
Test Failed:

Dave Boyer (DEP)
Witnessed By:

Comments:

MONARCH DRIVE

City of Littleton
Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal



On-Site Sewage Disposal

DEP has provided this form for use by on-site professionals and local Boards of Health. Other forms may be used, but the information must be substantially the same as provided here. Before using this form, check with your local Board of Health to determine the form they use.

JOB FILE
L/T-0007

A. Facility Information

1. Facility Information

Owner Name	<i>KATELFORD Development</i>		
Street Address	<i>Monarch Drive</i>		
City/Town	<i>LITTLETON MA</i>		
Map/Lot			
State			
Zip Code			

HAYES ENGINEERS, INC.
603 SALEM STREET
WAKEFIELD MA 01880
TEL: 781-22800
FAX: 781-67596

B. Site Information

1. (Check one) New Construction Upgrade Repair
2. Published Soil Survey available? Yes No If yes: Soil Name Year Published Publication Scale Soil Map Unit
3. Surficial Geological Report available? Yes No If yes: Geologic Material Year Published Publication Scale Map Unit
4. Flood Rate Insurance Map:
Above the 500 year flood boundary? Yes No
Within the 500 year flood boundary? Yes No
Within the 100 year flood boundary? Yes No
Within a Velocity Zone? Yes No
5. Wetland Area: National Wetland Inventory Map
Wetlands Conservancy Program Map
Map Unit Map Unit Name
6. Current Water Resource Conditions (USGS)
Map Unit Map Unit Name
7. Other references reviewed:
Range: Above Normal Normal Below Normal

Commonwealth of Massachusetts
City/Town of _____
Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal



D. Determination of High Groundwater Elevation

1. Method used:

- Depth observed standing water in observation hole A. _____ inches
- Depth weeping from side of observation hole A. _____ inches
- Depth to soil redoximorphic features (mottles) A. _____ inches
- Groundwater adjustment (USGS methodology) A. _____ inches

2. Index Well Number _____ Reading Date _____ Index Well Level _____
Adjustment Factor _____ Adjusted Groundwater Level _____

E. Depth of Pervious Material

1. Depth of Naturally Occurring Pervious Material

- a. Does at least four feet of naturally occurring pervious material exist in all areas observed throughout the area proposed for the soil absorption system? Yes No
- b. If yes, at what depth was it observed? Upper boundary: _____ inches Lower boundary: _____ inches

F. Certification

I certify that I am currently approved by the Department of Environmental Protection pursuant to 310 CMR 15.017 to conduct soil evaluations and that the above analysis has been performed by me consistent with the required training, expertise and experience described in 310 CMR 15.017. I further certify that the results of my soil evaluation, as indicated in the attached Soil Evaluation Form, are accurate and in accordance with 310 CMR 15.100 through 15.107.

Signature of Soil Evaluator
Gordon Rogerson
Typed or Printed Name of Soil Evaluator/License Number
SE 2074

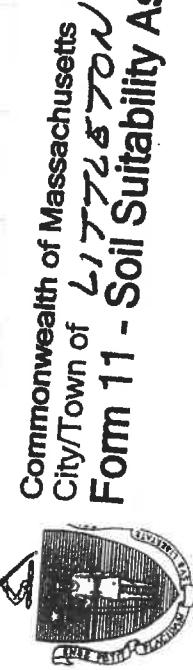
Date
Nov. 1994

*Date of Soil Evaluator Exam

Name of Board of Health Witness

Board of Health

Note: In accordance with 310 CMR 15.018(2) this form must be submitted to the approving authority within 60 days of the date of field testing, and to the designer and the property owner with Percolation Test Form 12.



Commonwealth of Massachusetts
City/Town of *LEWISTON*
Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

C. On-Site Review (Cont.)

Deep Observation Hole Number: 460

1. Location

Ground Elevation at Surface of Hole _____

Location (Identify on Plan) _____

Date 4-8-08

Time _____

Weather Sunny

50°

2. Land Use: Field

(e.g. woodland, agricultural field, vacant lot, etc.)

grass

Vegetation

Depth 10

Surface Stones

A

Slope (%)

Position on Landscape (attach sheet)

Landform

Surface Stones

Possible Wet Area

10

feet

Other _____

feet

feet

feet

feet

feet

feet

feet

feet

feet

3. Distances from: Open Water Body feet Drainage Way feet Possible Wet Area feet
Property Line feet Drinking Water Well feet Other _____

feet

4. Parent Material: Glacial Outwash

If Yes: Disturbed Soil Fill Material Impervious Layer(s) Weathered/Fractured Rock Bedrock
If No: No

5. Groundwater Observed: Yes No
If Yes: Depth Weeping from Pit 84 Depth Standing Water in Hole 84

Estimated Depth to High Groundwater: 84 inches elevation _____



**Commonwealth of Massachusetts
City/Town of LINTON
Form 11 - Soil Suitability /**

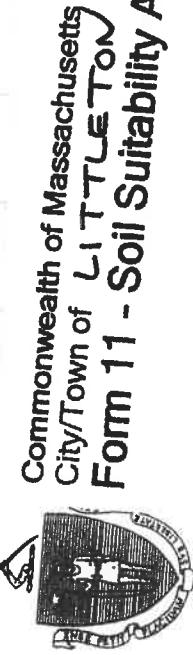
Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

Deep Observation Hole Number: _____

465

Depth (in.)	Soil Horizon/ Layer	Soil Matrix: Color-Moist (Munsell)	Redoximorphic Features (mottles)			Soil Texture (USDA)	Coarse Fragments % by Volume	Soil Structure	Soil Consistence (Moist)	Other
			Depth	Color	Percent					
0- 32	C ₁	10YR 5/6				gr CS	45	%	59	mh
32- 108	C ₂	2.5Y 6/3	84			CS	20	%	59	mh

Additional Notes



Commonwealth of Massachusetts
City/Town of LITTLETON
Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

C. On-Site Review (Cont.)

Deep Observation Hole Number: Hole 4-8-08

1. Location

Ground Elevation at Surface of Hole _____

Location (Identify on Plan) _____

Date

Sunny

Weather

Sunny

Weather

2. Land Use: Field

(e.g. woodland, agricultural field, vacant lot, etc.)

Vegetation

Landform

A

Slope (%)

10

Surface Stones

10

Slope (%)

Position on landscape (attach sheet)

10

Surface Stones

10

Slope (%)

Position on landscape (attach sheet)

10

Surface Stones

10

Slope (%)

Position on landscape (attach sheet)

10

Surface Stones

10

Slope (%)

Position on landscape (attach sheet)

10

Surface Stones

10

Slope (%)

Position on landscape (attach sheet)

10

Surface Stones

10

Slope (%)

Position on landscape (attach sheet)

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Surface Stones

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Slope (%)

Position on landscape (attach sheet)

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Surface Stones

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Slope (%)

Position on landscape (attach sheet)

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Surface Stones

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Slope (%)

Position on landscape (attach sheet)

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Surface Stones

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Slope (%)

Position on landscape (attach sheet)

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Slope (%)

Position on landscape (attach sheet)

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Surface Stones

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Slope (%)

Position on landscape (attach sheet)

10

Surface Stones

10

Slope (%)

Position on landscape (attach sheet)

10

Surface Stones

10

Slope (%)

Position on landscape (attach sheet)

10

Surface Stones

10

Slope (%)

Position on landscape (attach sheet)

10

Surface Stones

10

Slope (%)

Position on landscape (attach sheet)

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Surface Stones

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Slope (%)

Position on landscape (attach sheet)

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Surface Stones

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Slope (%)

Position on landscape (attach sheet)

10

Surface Stones

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Slope (%)

Position on landscape (attach sheet)

10

Surface Stones

10

Slope (%)

Position on landscape (attach sheet)

10

Surface



**Commonwealth of Massachusetts
City/Town of LITTLETON
Form 11 - Soil Suitability /**

Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

Deep Observation Hole Number: 466

Depth (in.)	Soil Horizon/ Layer	Soil Matrix: Color-Moist (Munsell)	Redoximorphic Features (mottles)		Soil Texture (USDA)	Coarse Fragments % by Volume		Soil Structure	Soil Consistence (Moist)	Other
			Depth	Color		Percent	Gravel			
0- 30	C ₁	10YR 5/6			gr CS	45	0%	39	mf	
30 96	C ₂	2.5Y 6/3	72		CS	35	0%	39	mf	

Additional Notes -



Commonwealth of Massachusetts
City/Town of LITTLETON
Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

C. On-Site Review (Cont.)

Deep Observation Hole Number: 462 4-8-08

1. Location	Date	Time	<u>Sunny 50°</u> Weather				
Ground Elevation at Surface of Hole							
Location (Identify on Plan)							
2. Land Use: <u>Field</u> (e.g. woodland, agricultural field, vacant lot, etc.)	Vegetation	Landform	Surface Stones	Slope (%)			
			<u>0°</u>	<u>A</u>			
3. Distances from:	Open Water Body	feet	Drainage Way	feet	Possible Wet Area	feet	Position on landscape (attach sheet)
Property Line	feet		Drinking Water Well	feet	feet		
4. Parent Material: <u>Glacial Drift and Wash</u>							
If Yes:	Disturbed Soil <input type="checkbox"/>	Fill Material <input type="checkbox"/>	Impervious Layer(s) <input type="checkbox"/>	Unsuitable Materials Present:	Yes <input type="checkbox"/>	No <input checked="" type="checkbox"/>	
5. Groundwater Observed:	Yes <input checked="" type="checkbox"/>	No <input type="checkbox"/>	Weathered/Fractured Rock <input type="checkbox"/>	Bedrock <input type="checkbox"/>			
If Yes:	Depth Weeping from Pit	<u>68</u> inches	Depth Standing Water in Hole	<u>68</u> inches			
Estimated Depth to High Groundwater:							



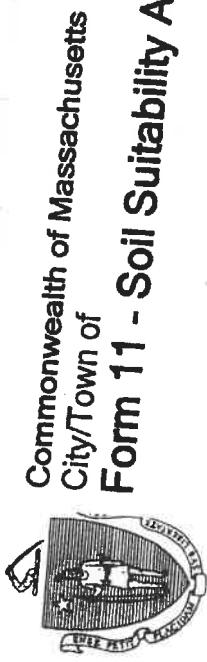
Commonwealth of Massachusetts
City/Town of LITTLETON
Form 11 - Soil Suitability /

City/Town of LITTLERIDGE Soil Suitability Assessment for On-Site Sewage Disposal

467
Soil Observation Hole Number:

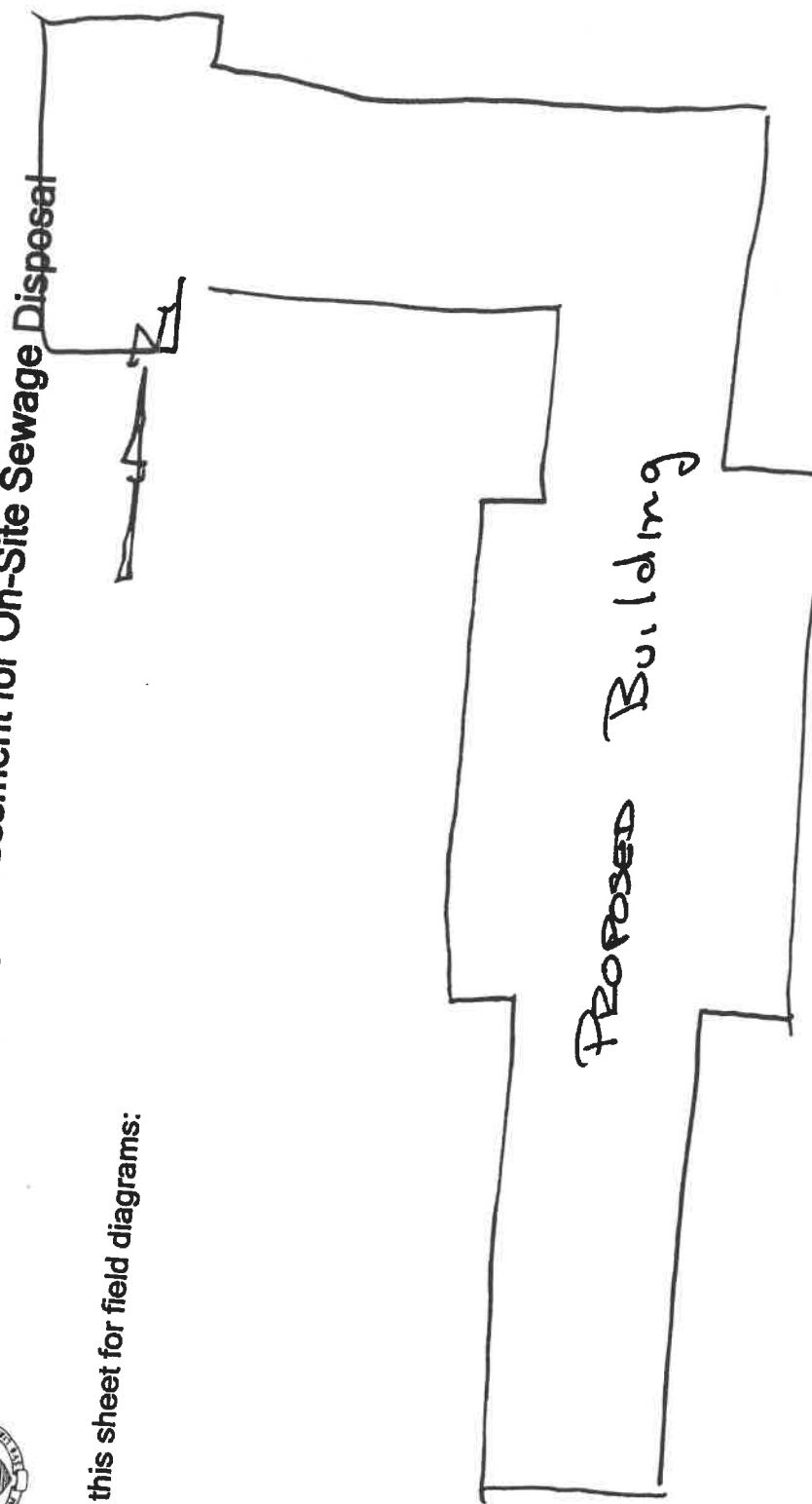
Depth (in.)	Soil Horizon/ Layer	Soil Matrix: Color-Moist (Munsell)	Redoximorphic Features (mottles)		Soil Texture (USDA)	Coarse Fragments % by Volume		Soil Structure	Soil Consistency (Moist)	Other
			Depth	Color		Percent	Gravel			
0 - 10	C ₁	10YR 5/6			grcs	25	0%	5%	mu	
10 - 72	C ₂	2.5Y 6/3	68		cs	35	0%	5%	mu	
72 - 90	C ₃	10YR 4/2			w grcy	50	0%	5%	mu	

Additional Notes



Commonwealth of Massachusetts
City/Town of
Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

Use this sheet for field diagrams:



465 460 867

HydroCAD Data



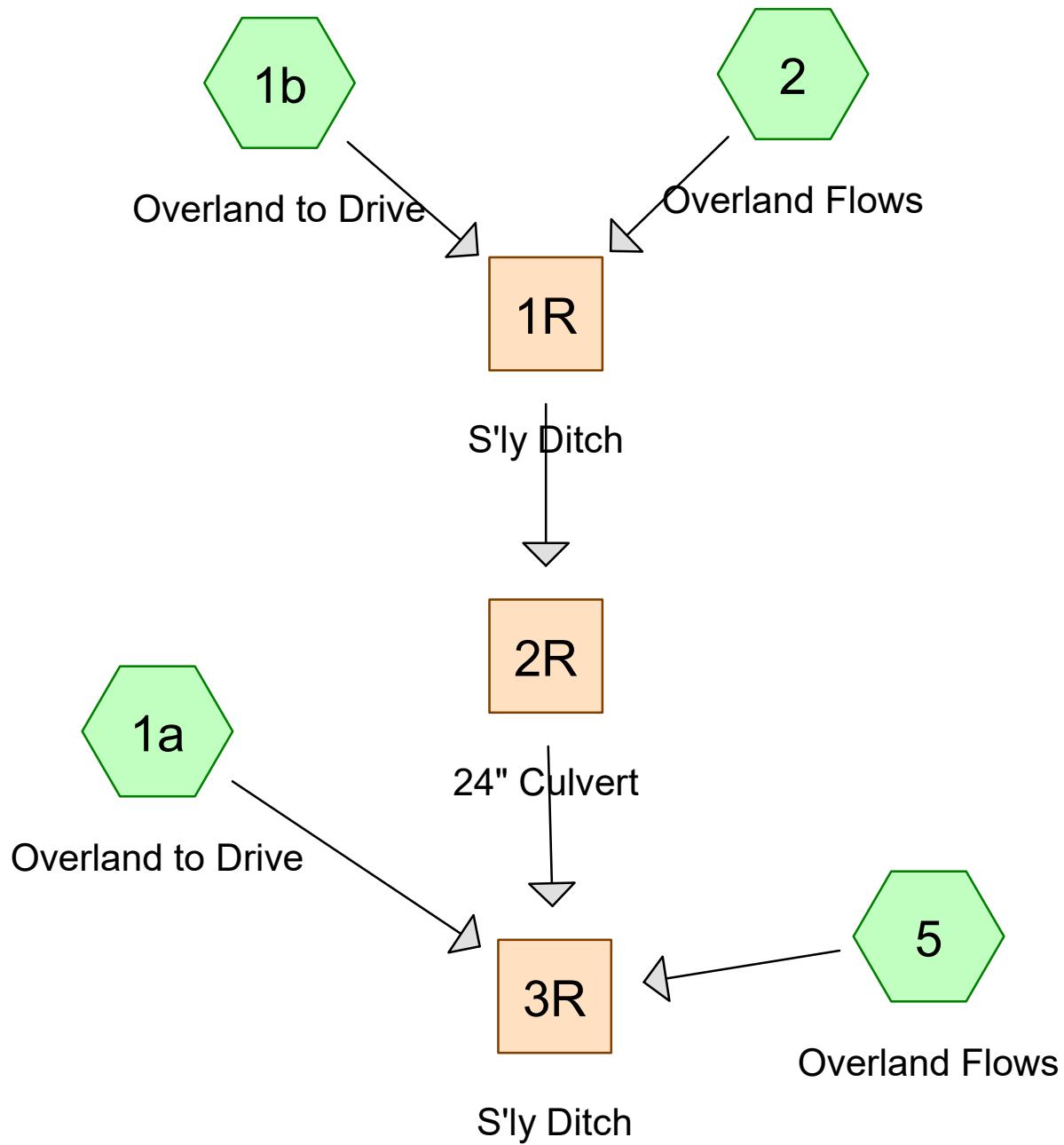
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PRE-DEVELOPMENT

DRAINAGE CALCULATIONS



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Rainfall Events Listing (selected events)

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	2-yr	NRCC 24-hr	D	Default	24.00	1	3.19	2
2	10-yr	NRCC 24-hr	D	Default	24.00	1	4.92	2
3	100-yr	NRCC 24-hr	D	Default	24.00	1	7.66	2

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Area Listing (all nodes)

Area (sq-ft)	CN	Description (subcatchment-numbers)
9,500	39	>75% Grass cover, Good, HSG A (1a, 1b, 2)
279,675	48	Brush, Poor, HSG A (1a, 1b, 2, 5)
5,325	72	Dirt roads, HSG A (1a, 1b, 2, 5)
71,115	36	Woods, Fair, HSG A (1a, 1b, 2, 5)
365,615	46	TOTAL AREA

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Soil Listing (all nodes)

Area (sq-ft)	Soil Group	Subcatchment Numbers
365,615	HSG A	1a, 1b, 2, 5
0	HSG B	
0	HSG C	
0	HSG D	
0	Other	
365,615		TOTAL AREA

Summary for Subcatchment 1a: Overland to Drive

Runoff = 0.01 cfs @ 14.35 hrs, Volume= 213 cf, Depth= 0.11"
 Routed to Reach 3R : S'ly Ditch

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
 NRCC 24-hr D 2-yr Rainfall=3.19"

Area (sf)	CN	Description
575	36	Woods, Fair, HSG A
21,680	48	Brush, Poor, HSG A
375	39	>75% Grass cover, Good, HSG A
1,320	72	Dirt roads, HSG A
23,950	49	Weighted Average
23,950		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.9	50	0.0060	0.21		Sheet Flow, Fallow n= 0.050 P2= 3.00"
1.1	95	0.0200	1.41		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
0.3	50	0.0200	2.87		Shallow Concentrated Flow, Paved Kv= 20.3 fps
1.5	266		3.00		Direct Entry, Pipe Flow
6.8	461	Total			

Summary for Subcatchment 1b: Overland to Drive

Runoff = 0.00 cfs @ 24.02 hrs, Volume= 41 cf, Depth= 0.03"
 Routed to Reach 1R : S'ly Ditch

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
 NRCC 24-hr D 2-yr Rainfall=3.19"

Area (sf)	CN	Description
2,300	36	Woods, Fair, HSG A
8,580	48	Brush, Poor, HSG A
4,700	39	>75% Grass cover, Good, HSG A
200	72	Dirt roads, HSG A
15,780	44	Weighted Average
15,780		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.9	50	0.0060	0.21		Sheet Flow, Fallow n= 0.050 P2= 3.00"
1.4	115	0.0200	1.41		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
3.3	405	0.0100	2.03		Shallow Concentrated Flow, Paved Kv= 20.3 fps
0.4	65		3.00		Direct Entry, Pipe flow
9.0	635	Total			

Summary for Subcatchment 2: Overland Flows

Runoff = 0.03 cfs @ 22.24 hrs, Volume= 895 cf, Depth= 0.06"
Routed to Reach 1R : S'ly Ditch

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
NRCC 24-hr D 2-yr Rainfall=3.19"

Area (sf)	CN	Description
38,225	36	Woods, Fair, HSG A
144,680	48	Brush, Poor, HSG A
4,425	39	>75% Grass cover, Good, HSG A
3,165	72	Dirt roads, HSG A
190,495	46	Weighted Average
190,495		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.2	50	0.0240	0.37		Sheet Flow, Fallow n= 0.050 P2= 3.00"
1.7	115	0.0120	1.10		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
2.1	45	0.0013	0.36		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
0.1	20	0.2700	5.20		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
6.1	230	Total			

Summary for Subcatchment 5: Overland Flows

Runoff = 0.02 cfs @ 22.59 hrs, Volume= 484 cf, Depth= 0.04"
Routed to Reach 3R : S'ly Ditch

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
NRCC 24-hr D 2-yr Rainfall=3.19"

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NRCC 24-hr D 2-yr Rainfall=3.19"

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Area (sf)	CN	Description			
30,015	36	Woods, Fair, HSG A			
104,735	48	Brush, Poor, HSG A			
640	72	Dirt roads, HSG A			
135,390	45	Weighted Average			
135,390		100.00% Pervious Area			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.4	50	0.0200	0.35		Sheet Flow, Fallow n= 0.050 P2= 3.00"
0.2	30	0.1100	3.32		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
7.4	280	0.0040	0.63		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
0.1	30	0.1600	4.00		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
10.1	390	Total			

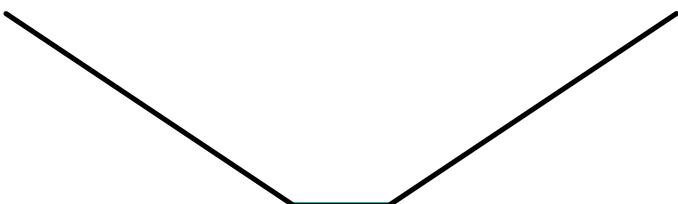
Summary for Reach 1R: S'ly Ditch

Inflow Area = 206,275 sf, 0.00% Impervious, Inflow Depth = 0.05" for 2-yr event
 Inflow = 0.03 cfs @ 22.24 hrs, Volume= 936 cf
 Outflow = 0.03 cfs @ 26.45 hrs, Volume= 856 cf, Atten= 2%, Lag= 252.6 min
 Routed to Reach 2R : 24" Culvert

Routing by Stor-Ind+Trans method, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
 Max. Velocity= 0.09 fps, Min. Travel Time= 145.6 min
 Avg. Velocity = 0.07 fps, Avg. Travel Time= 176.9 min

Peak Storage= 238 cf @ 24.03 hrs
 Average Depth at Peak Storage= 0.10' , Surface Width= 3.30'
 Bank-Full Depth= 6.00' Flow Area= 72.0 sf, Capacity= 58.69 cfs

3.00' x 6.00' deep channel, n= 0.100 Earth, dense brush, high stage
 Side Slope Z-value= 1.5 '/' Top Width= 21.00'
 Length= 750.0' Slope= 0.0007 '/'
 Inlet Invert= 224.00', Outlet Invert= 223.46'



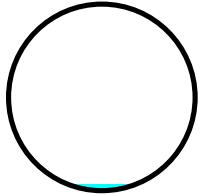
Summary for Reach 2R: 24" Culvert

Inflow Area = 206,275 sf, 0.00% Impervious, Inflow Depth > 0.05" for 2-yr event
Inflow = 0.03 cfs @ 26.45 hrs, Volume= 856 cf
Outflow = 0.03 cfs @ 26.50 hrs, Volume= 854 cf, Atten= 0%, Lag= 2.9 min
Routed to Reach 3R : S'ly Ditch

Routing by Stor-Ind+Trans method, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
Max. Velocity= 0.77 fps, Min. Travel Time= 2.3 min
Avg. Velocity = 0.64 fps, Avg. Travel Time= 2.7 min

Peak Storage= 4 cf @ 26.47 hrs
Average Depth at Peak Storage= 0.07' , Surface Width= 0.74'
Bank-Full Depth= 2.00' Flow Area= 3.1 sf, Capacity= 11.72 cfs

24.0" Round Pipe
n= 0.012 Concrete pipe, finished
Length= 105.0' Slope= 0.0023 '/'
Inlet Invert= 223.46', Outlet Invert= 223.22'

**Summary for Reach 3R: S'ly Ditch**

Inflow Area = 365,615 sf, 0.00% Impervious, Inflow Depth > 0.05" for 2-yr event
Inflow = 0.05 cfs @ 24.02 hrs, Volume= 1,550 cf
Outflow = 0.04 cfs @ 26.63 hrs, Volume= 1,169 cf, Atten= 8%, Lag= 156.6 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
Max. Velocity= 0.08 fps, Min. Travel Time= 152.6 min
Avg. Velocity = 0.06 fps, Avg. Travel Time= 199.8 min

Peak Storage= 392 cf @ 24.09 hrs
Average Depth at Peak Storage= 0.17' , Surface Width= 3.52'
Bank-Full Depth= 6.00' Flow Area= 72.0 sf, Capacity= 38.78 cfs

3.00' x 6.00' deep channel, n= 0.100 Earth, dense brush, high stage
Side Slope Z-value= 1.5 '/' Top Width= 21.00'
Length= 700.0' Slope= 0.0003 '/'
Inlet Invert= 223.22', Outlet Invert= 223.00'

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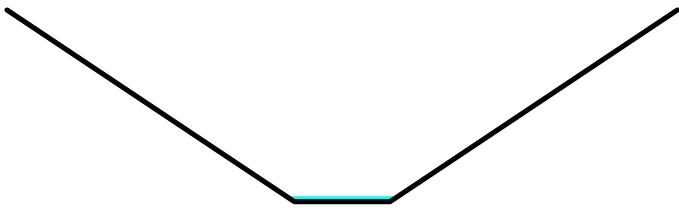
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NRCC 24-hr D 2-yr Rainfall=3.19"

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Summary for Subcatchment 1a: Overland to Drive

Runoff = 0.22 cfs @ 12.16 hrs, Volume= 1,214 cf, Depth= 0.61"
 Routed to Reach 3R : S'ly Ditch

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
 NRCC 24-hr D 10-yr Rainfall=4.92"

Area (sf)	CN	Description
575	36	Woods, Fair, HSG A
21,680	48	Brush, Poor, HSG A
375	39	>75% Grass cover, Good, HSG A
1,320	72	Dirt roads, HSG A
23,950	49	Weighted Average
23,950		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.9	50	0.0060	0.21		Sheet Flow, Fallow n= 0.050 P2= 3.00"
1.1	95	0.0200	1.41		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
0.3	50	0.0200	2.87		Shallow Concentrated Flow, Paved Kv= 20.3 fps
1.5	266		3.00		Direct Entry, Pipe Flow
6.8	461	Total			

Summary for Subcatchment 1b: Overland to Drive

Runoff = 0.03 cfs @ 12.29 hrs, Volume= 491 cf, Depth= 0.37"
 Routed to Reach 1R : S'ly Ditch

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
 NRCC 24-hr D 10-yr Rainfall=4.92"

Area (sf)	CN	Description
2,300	36	Woods, Fair, HSG A
8,580	48	Brush, Poor, HSG A
4,700	39	>75% Grass cover, Good, HSG A
200	72	Dirt roads, HSG A
15,780	44	Weighted Average
15,780		100.00% Pervious Area

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NRCC 24-hr D 10-yr Rainfall=4.92"

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.9	50	0.0060	0.21		Sheet Flow, Fallow n= 0.050 P2= 3.00"
1.4	115	0.0200	1.41		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
3.3	405	0.0100	2.03		Shallow Concentrated Flow, Paved Kv= 20.3 fps
0.4	65		3.00		Direct Entry, Pipe flow
9.0	635	Total			

Summary for Subcatchment 2: Overland Flows

Runoff = 0.90 cfs @ 12.16 hrs, Volume= 7,339 cf, Depth= 0.46"
 Routed to Reach 1R : S'ly Ditch

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
 NRCC 24-hr D 10-yr Rainfall=4.92"

Area (sf)	CN	Description
38,225	36	Woods, Fair, HSG A
144,680	48	Brush, Poor, HSG A
4,425	39	>75% Grass cover, Good, HSG A
3,165	72	Dirt roads, HSG A
190,495	46	Weighted Average
190,495		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.2	50	0.0240	0.37		Sheet Flow, Fallow n= 0.050 P2= 3.00"
1.7	115	0.0120	1.10		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
2.1	45	0.0013	0.36		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
0.1	20	0.2700	5.20		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
6.1	230	Total			

Summary for Subcatchment 5: Overland Flows

Runoff = 0.38 cfs @ 12.26 hrs, Volume= 4,704 cf, Depth= 0.42"
 Routed to Reach 3R : S'ly Ditch

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
 NRCC 24-hr D 10-yr Rainfall=4.92"

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Area (sf)	CN	Description			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
30,015	36	Woods, Fair, HSG A			
104,735	48	Brush, Poor, HSG A			
640	72	Dirt roads, HSG A			
135,390	45	Weighted Average			
135,390		100.00% Pervious Area			
2.4	50	0.0200	0.35		Sheet Flow, Fallow n= 0.050 P2= 3.00"
0.2	30	0.1100	3.32		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
7.4	280	0.0040	0.63		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
0.1	30	0.1600	4.00		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
10.1	390	Total			

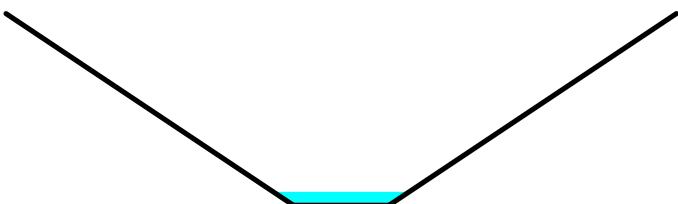
Summary for Reach 1R: S'ly Ditch

Inflow Area = 206,275 sf, 0.00% Impervious, Inflow Depth = 0.46" for 10-yr event
 Inflow = 0.92 cfs @ 12.16 hrs, Volume= 7,830 cf
 Outflow = 0.29 cfs @ 14.43 hrs, Volume= 7,739 cf, Atten= 68%, Lag= 136.2 min
 Routed to Reach 2R : 24" Culvert

Routing by Stor-Ind+Trans method, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
 Max. Velocity= 0.19 fps, Min. Travel Time= 64.8 min
 Avg. Velocity = 0.13 fps, Avg. Travel Time= 95.1 min

Peak Storage= 1,139 cf @ 13.35 hrs
 Average Depth at Peak Storage= 0.42' , Surface Width= 4.26'
 Bank-Full Depth= 6.00' Flow Area= 72.0 sf, Capacity= 58.69 cfs

3.00' x 6.00' deep channel, n= 0.100 Earth, dense brush, high stage
 Side Slope Z-value= 1.5 '/' Top Width= 21.00'
 Length= 750.0' Slope= 0.0007 '/'
 Inlet Invert= 224.00', Outlet Invert= 223.46'



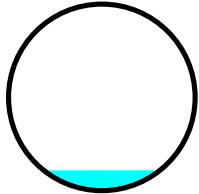
Summary for Reach 2R: 24" Culvert

Inflow Area = 206,275 sf, 0.00% Impervious, Inflow Depth > 0.45" for 10-yr event
Inflow = 0.29 cfs @ 14.43 hrs, Volume= 7,739 cf
Outflow = 0.29 cfs @ 14.46 hrs, Volume= 7,738 cf, Atten= 0%, Lag= 1.8 min
Routed to Reach 3R : S'ly Ditch

Routing by Stor-Ind+Trans method, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
Max. Velocity= 1.58 fps, Min. Travel Time= 1.1 min
Avg. Velocity = 1.15 fps, Avg. Travel Time= 1.5 min

Peak Storage= 19 cf @ 14.45 hrs
Average Depth at Peak Storage= 0.22' , Surface Width= 1.25'
Bank-Full Depth= 2.00' Flow Area= 3.1 sf, Capacity= 11.72 cfs

24.0" Round Pipe
n= 0.012 Concrete pipe, finished
Length= 105.0' Slope= 0.0023 '/'
Inlet Invert= 223.46', Outlet Invert= 223.22'

**Summary for Reach 3R: S'ly Ditch**

Inflow Area = 365,615 sf, 0.00% Impervious, Inflow Depth > 0.45" for 10-yr event
Inflow = 0.53 cfs @ 12.23 hrs, Volume= 13,656 cf
Outflow = 0.40 cfs @ 16.49 hrs, Volume= 13,282 cf, Atten= 25%, Lag= 255.6 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
Max. Velocity= 0.16 fps, Min. Travel Time= 73.0 min
Avg. Velocity = 0.12 fps, Avg. Travel Time= 94.7 min

Peak Storage= 1,741 cf @ 15.27 hrs
Average Depth at Peak Storage= 0.63' , Surface Width= 4.89'
Bank-Full Depth= 6.00' Flow Area= 72.0 sf, Capacity= 38.78 cfs

3.00' x 6.00' deep channel, n= 0.100 Earth, dense brush, high stage
Side Slope Z-value= 1.5 '/' Top Width= 21.00'
Length= 700.0' Slope= 0.0003 '/'
Inlet Invert= 223.22', Outlet Invert= 223.00'

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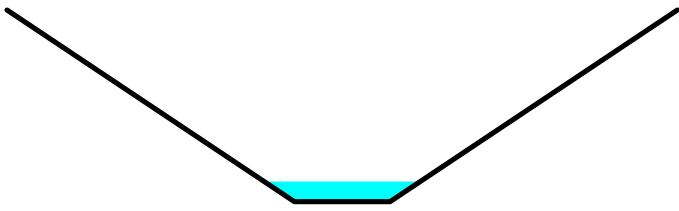
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NRCC 24-hr D 10-yr Rainfall=4.92"

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Summary for Subcatchment 1a: Overland to Drive

Runoff = 1.07 cfs @ 12.15 hrs, Volume= 3,885 cf, Depth= 1.95"
 Routed to Reach 3R : S'ly Ditch

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
 NRCC 24-hr D 100-yr Rainfall=7.66"

Area (sf)	CN	Description
575	36	Woods, Fair, HSG A
21,680	48	Brush, Poor, HSG A
375	39	>75% Grass cover, Good, HSG A
1,320	72	Dirt roads, HSG A
23,950	49	Weighted Average
23,950		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.9	50	0.0060	0.21		Sheet Flow, Fallow n= 0.050 P2= 3.00"
1.1	95	0.0200	1.41		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
0.3	50	0.0200	2.87		Shallow Concentrated Flow, Paved Kv= 20.3 fps
1.5	266		3.00		Direct Entry, Pipe Flow
6.8	461	Total			

Summary for Subcatchment 1b: Overland to Drive

Runoff = 0.43 cfs @ 12.17 hrs, Volume= 1,928 cf, Depth= 1.47"
 Routed to Reach 1R : S'ly Ditch

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
 NRCC 24-hr D 100-yr Rainfall=7.66"

Area (sf)	CN	Description
2,300	36	Woods, Fair, HSG A
8,580	48	Brush, Poor, HSG A
4,700	39	>75% Grass cover, Good, HSG A
200	72	Dirt roads, HSG A
15,780	44	Weighted Average
15,780		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.9	50	0.0060	0.21		Sheet Flow, Fallow n= 0.050 P2= 3.00"
1.4	115	0.0200	1.41		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
3.3	405	0.0100	2.03		Shallow Concentrated Flow, Paved Kv= 20.3 fps
0.4	65		3.00		Direct Entry, Pipe flow
9.0	635	Total			

Summary for Subcatchment 2: Overland Flows

Runoff = 7.10 cfs @ 12.14 hrs, Volume= 26,272 cf, Depth= 1.65"
Routed to Reach 1R : S'ly Ditch

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
NRCC 24-hr D 100-yr Rainfall=7.66"

Area (sf)	CN	Description
38,225	36	Woods, Fair, HSG A
144,680	48	Brush, Poor, HSG A
4,425	39	>75% Grass cover, Good, HSG A
3,165	72	Dirt roads, HSG A
190,495	46	Weighted Average
190,495		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.2	50	0.0240	0.37		Sheet Flow, Fallow n= 0.050 P2= 3.00"
1.7	115	0.0120	1.10		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
2.1	45	0.0013	0.36		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
0.1	20	0.2700	5.20		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
6.1	230	Total			

Summary for Subcatchment 5: Overland Flows

Runoff = 3.86 cfs @ 12.19 hrs, Volume= 17,600 cf, Depth= 1.56"
Routed to Reach 3R : S'ly Ditch

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
NRCC 24-hr D 100-yr Rainfall=7.66"

Area (sf)	CN	Description			
30,015	36	Woods, Fair, HSG A			
104,735	48	Brush, Poor, HSG A			
640	72	Dirt roads, HSG A			
135,390	45	Weighted Average			
135,390		100.00% Pervious Area			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.4	50	0.0200	0.35		Sheet Flow, Fallow n= 0.050 P2= 3.00"
0.2	30	0.1100	3.32		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
7.4	280	0.0040	0.63		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
0.1	30	0.1600	4.00		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
10.1	390	Total			

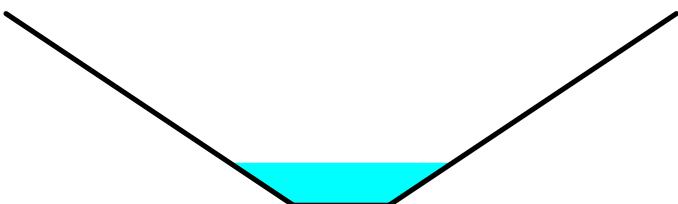
Summary for Reach 1R: S'ly Ditch

Inflow Area = 206,275 sf, 0.00% Impervious, Inflow Depth = 1.64" for 100-yr event
 Inflow = 7.50 cfs @ 12.14 hrs, Volume= 28,200 cf
 Outflow = 2.41 cfs @ 12.96 hrs, Volume= 28,102 cf, Atten= 68%, Lag= 48.9 min
 Routed to Reach 2R : 24" Culvert

Routing by Stor-Ind+Trans method, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
 Max. Velocity= 0.36 fps, Min. Travel Time= 34.8 min
 Avg. Velocity = 0.18 fps, Avg. Travel Time= 68.7 min

Peak Storage= 5,020 cf @ 12.38 hrs
 Average Depth at Peak Storage= 1.34' , Surface Width= 7.01'
 Bank-Full Depth= 6.00' Flow Area= 72.0 sf, Capacity= 58.69 cfs

3.00' x 6.00' deep channel, n= 0.100 Earth, dense brush, high stage
 Side Slope Z-value= 1.5 '/' Top Width= 21.00'
 Length= 750.0' Slope= 0.0007 '/'
 Inlet Invert= 224.00', Outlet Invert= 223.46'



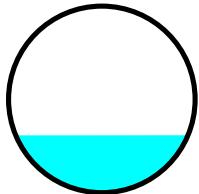
Summary for Reach 2R: 24" Culvert

Inflow Area = 206,275 sf, 0.00% Impervious, Inflow Depth > 1.63" for 100-yr event
Inflow = 2.41 cfs @ 12.96 hrs, Volume= 28,102 cf
Outflow = 2.41 cfs @ 12.97 hrs, Volume= 28,100 cf, Atten= 0%, Lag= 1.0 min
Routed to Reach 3R : S'ly Ditch

Routing by Stor-Ind+Trans method, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
Max. Velocity= 2.93 fps, Min. Travel Time= 0.6 min
Avg. Velocity = 1.54 fps, Avg. Travel Time= 1.1 min

Peak Storage= 86 cf @ 12.96 hrs
Average Depth at Peak Storage= 0.61', Surface Width= 1.85'
Bank-Full Depth= 2.00' Flow Area= 3.1 sf, Capacity= 11.72 cfs

24.0" Round Pipe
n= 0.012 Concrete pipe, finished
Length= 105.0' Slope= 0.0023 '/'
Inlet Invert= 223.46', Outlet Invert= 223.22'

**Summary for Reach 3R: S'ly Ditch**

Inflow Area = 365,615 sf, 0.00% Impervious, Inflow Depth > 1.63" for 100-yr event
Inflow = 4.80 cfs @ 12.18 hrs, Volume= 49,585 cf
Outflow = 2.60 cfs @ 14.17 hrs, Volume= 49,220 cf, Atten= 46%, Lag= 119.3 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
Max. Velocity= 0.27 fps, Min. Travel Time= 43.1 min
Avg. Velocity = 0.17 fps, Avg. Travel Time= 69.9 min

Peak Storage= 6,709 cf @ 13.45 hrs
Average Depth at Peak Storage= 1.72', Surface Width= 8.15'
Bank-Full Depth= 6.00' Flow Area= 72.0 sf, Capacity= 38.78 cfs

3.00' x 6.00' deep channel, n= 0.100 Earth, dense brush, high stage
Side Slope Z-value= 1.5 '/' Top Width= 21.00'
Length= 700.0' Slope= 0.0003 '/'
Inlet Invert= 223.22', Outlet Invert= 223.00'

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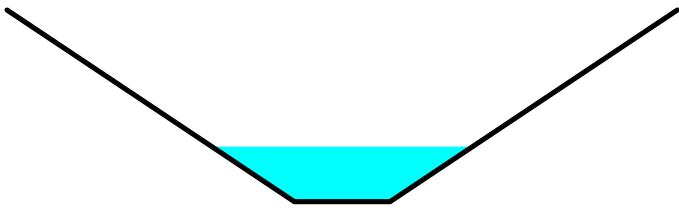
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NRCC 24-hr D 100-yr Rainfall=7.66"

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25-YEAR Pre-Development - Detailed

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Page 1

Rainfall Events Listing (selected events)

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	25-yr	NRCC 24-hr	D	Default	24.00	1	6.00	2

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Area Listing (all nodes)

Area (sq-ft)	CN	Description (subcatchment-numbers)
9,500	39	>75% Grass cover, Good, HSG A (1a, 1b, 2)
279,675	48	Brush, Poor, HSG A (1a, 1b, 2, 5)
5,325	72	Dirt roads, HSG A (1a, 1b, 2, 5)
71,115	36	Woods, Fair, HSG A (1a, 1b, 2, 5)
365,615	46	TOTAL AREA

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Soil Listing (all nodes)

Area (sq-ft)	Soil Group	Subcatchment Numbers
365,615	HSG A	1a, 1b, 2, 5
0	HSG B	
0	HSG C	
0	HSG D	
0	Other	
365,615		TOTAL AREA

Summary for Subcatchment 1a: Overland to Drive

Runoff = 0.51 cfs @ 12.15 hrs, Volume= 2,139 cf, Depth= 1.07"
 Routed to Reach 3R : S'ly Ditch

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
 NRCC 24-hr D 25-yr Rainfall=6.00"

Area (sf)	CN	Description
575	36	Woods, Fair, HSG A
21,680	48	Brush, Poor, HSG A
375	39	>75% Grass cover, Good, HSG A
1,320	72	Dirt roads, HSG A
23,950	49	Weighted Average
23,950		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.9	50	0.0060	0.21		Sheet Flow, Fallow n= 0.050 P2= 3.00"
1.1	95	0.0200	1.41		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
0.3	50	0.0200	2.87		Shallow Concentrated Flow, Paved Kv= 20.3 fps
1.5	266		3.00		Direct Entry, Pipe Flow
6.8	461	Total			

Summary for Subcatchment 1b: Overland to Drive

Runoff = 0.15 cfs @ 12.19 hrs, Volume= 970 cf, Depth= 0.74"
 Routed to Reach 1R : S'ly Ditch

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
 NRCC 24-hr D 25-yr Rainfall=6.00"

Area (sf)	CN	Description
2,300	36	Woods, Fair, HSG A
8,580	48	Brush, Poor, HSG A
4,700	39	>75% Grass cover, Good, HSG A
200	72	Dirt roads, HSG A
15,780	44	Weighted Average
15,780		100.00% Pervious Area

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NRCC 24-hr D 25-yr Rainfall=6.00"

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.9	50	0.0060	0.21		Sheet Flow, Fallow n= 0.050 P2= 3.00"
1.4	115	0.0200	1.41		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
3.3	405	0.0100	2.03		Shallow Concentrated Flow, Paved Kv= 20.3 fps
0.4	65		3.00		Direct Entry, Pipe flow
9.0	635	Total			

Summary for Subcatchment 2: Overland Flows

Runoff = 2.99 cfs @ 12.15 hrs, Volume= 13,757 cf, Depth= 0.87"
 Routed to Reach 1R : S'ly Ditch

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
 NRCC 24-hr D 25-yr Rainfall=6.00"

Area (sf)	CN	Description
38,225	36	Woods, Fair, HSG A
144,680	48	Brush, Poor, HSG A
4,425	39	>75% Grass cover, Good, HSG A
3,165	72	Dirt roads, HSG A
190,495	46	Weighted Average
190,495		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.2	50	0.0240	0.37		Sheet Flow, Fallow n= 0.050 P2= 3.00"
1.7	115	0.0120	1.10		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
2.1	45	0.0013	0.36		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
0.1	20	0.2700	5.20		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
6.1	230	Total			

Summary for Subcatchment 5: Overland Flows

Runoff = 1.48 cfs @ 12.20 hrs, Volume= 9,040 cf, Depth= 0.80"
 Routed to Reach 3R : S'ly Ditch

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
 NRCC 24-hr D 25-yr Rainfall=6.00"

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NRCC 24-hr D 25-yr Rainfall=6.00"

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Area (sf)	CN	Description			
30,015	36	Woods, Fair, HSG A			
104,735	48	Brush, Poor, HSG A			
640	72	Dirt roads, HSG A			
135,390	45	Weighted Average			
135,390		100.00% Pervious Area			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.4	50	0.0200	0.35		Sheet Flow, Fallow n= 0.050 P2= 3.00"
0.2	30	0.1100	3.32		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
7.4	280	0.0040	0.63		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
0.1	30	0.1600	4.00		Shallow Concentrated Flow, Nearly Bare & Untilled Kv= 10.0 fps
10.1	390	Total			

Summary for Reach 1R: S'ly Ditch

Inflow Area = 206,275 sf, 0.00% Impervious, Inflow Depth = 0.86" for 25-yr event

Inflow = 3.12 cfs @ 12.15 hrs, Volume= 14,727 cf

Outflow = 0.81 cfs @ 13.43 hrs, Volume= 14,634 cf, Atten= 74%, Lag= 76.9 min

Routed to Reach 2R : 24" Culvert

Routing by Stor-Ind+Trans method, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs

Max. Velocity= 0.26 fps, Min. Travel Time= 47.3 min

Avg. Velocity = 0.16 fps, Avg. Travel Time= 80.1 min

Peak Storage= 2,295 cf @ 12.64 hrs

Average Depth at Peak Storage= 0.74' , Surface Width= 5.23'

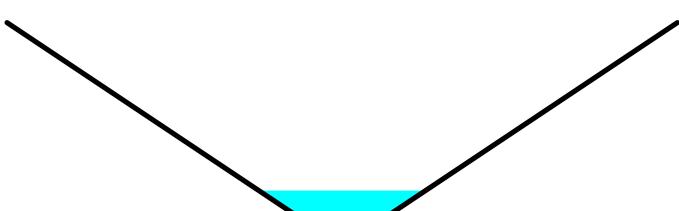
Bank-Full Depth= 6.00' Flow Area= 72.0 sf, Capacity= 58.69 cfs

3.00' x 6.00' deep channel, n= 0.100 Earth, dense brush, high stage

Side Slope Z-value= 1.5 '/' Top Width= 21.00'

Length= 750.0' Slope= 0.0007 '/'

Inlet Invert= 224.00', Outlet Invert= 223.46'



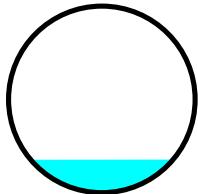
Summary for Reach 2R: 24" Culvert

Inflow Area = 206,275 sf, 0.00% Impervious, Inflow Depth > 0.85" for 25-yr event
Inflow = 0.81 cfs @ 13.43 hrs, Volume= 14,634 cf
Outflow = 0.81 cfs @ 13.45 hrs, Volume= 14,632 cf, Atten= 0%, Lag= 1.4 min
Routed to Reach 3R : S'ly Ditch

Routing by Stor-Ind+Trans method, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
Max. Velocity= 2.14 fps, Min. Travel Time= 0.8 min
Avg. Velocity = 1.34 fps, Avg. Travel Time= 1.3 min

Peak Storage= 40 cf @ 13.44 hrs
Average Depth at Peak Storage= 0.36' , Surface Width= 1.53'
Bank-Full Depth= 2.00' Flow Area= 3.1 sf, Capacity= 11.72 cfs

24.0" Round Pipe
n= 0.012 Concrete pipe, finished
Length= 105.0' Slope= 0.0023 '/'
Inlet Invert= 223.46', Outlet Invert= 223.22'

**Summary for Reach 3R: S'ly Ditch**

Inflow Area = 365,615 sf, 0.00% Impervious, Inflow Depth > 0.85" for 25-yr event
Inflow = 1.90 cfs @ 12.19 hrs, Volume= 25,811 cf
Outflow = 0.99 cfs @ 15.12 hrs, Volume= 25,446 cf, Atten= 48%, Lag= 175.9 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-30.00 hrs, dt= 0.01 hrs
Max. Velocity= 0.21 fps, Min. Travel Time= 56.0 min
Avg. Velocity = 0.15 fps, Avg. Travel Time= 80.2 min

Peak Storage= 3,316 cf @ 14.18 hrs
Average Depth at Peak Storage= 1.04' , Surface Width= 6.12'
Bank-Full Depth= 6.00' Flow Area= 72.0 sf, Capacity= 38.78 cfs

3.00' x 6.00' deep channel, n= 0.100 Earth, dense brush, high stage
Side Slope Z-value= 1.5 '/' Top Width= 21.00'
Length= 700.0' Slope= 0.0003 '/'
Inlet Invert= 223.22', Outlet Invert= 223.00'

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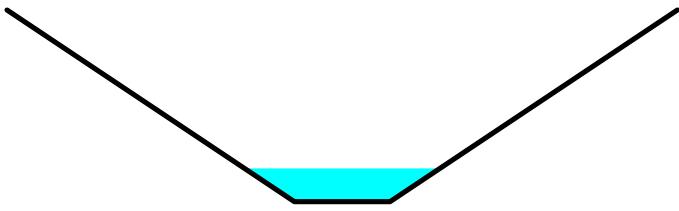
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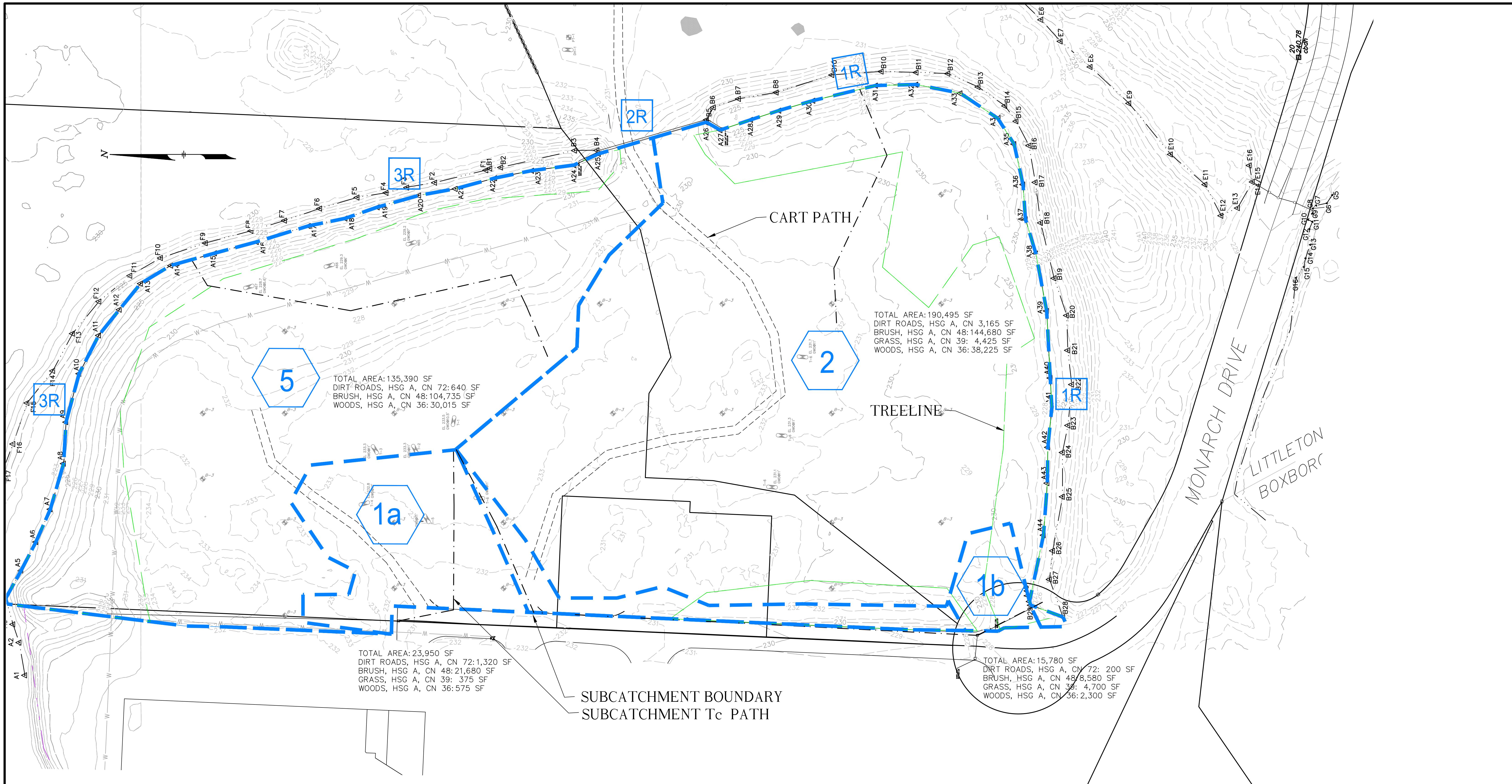
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POST-DEVELOPMENT

DRAINAGE CALCULATIONS



**PRE DEVELOPMENT
DRAINAGE PLAN**

LOCATION: MONARCH DRIVE
 CITY/TOWN: LITTLETON, MASSACHUSETTS
 PREPARED FOR:

VMD INDUSTRIES V LLC

SCALE: 1"=60' DATE: APRIL 2022

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PROJECT No.: 5554

PLAN No.: 5554-PRE



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